

# Loading path for a structure



**Code\_Aster, Salome-Meca course material**

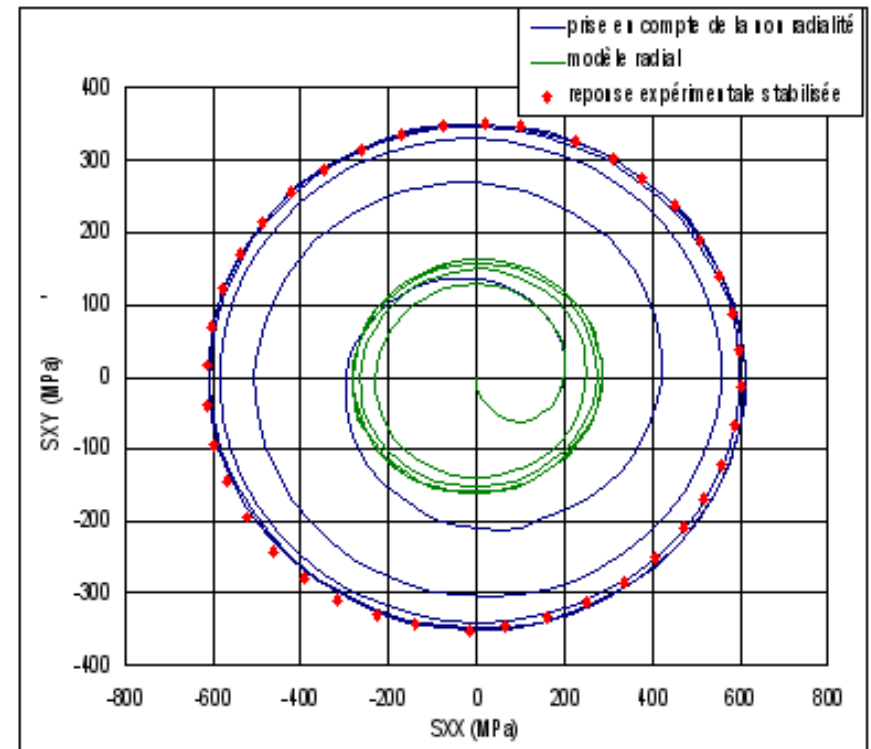
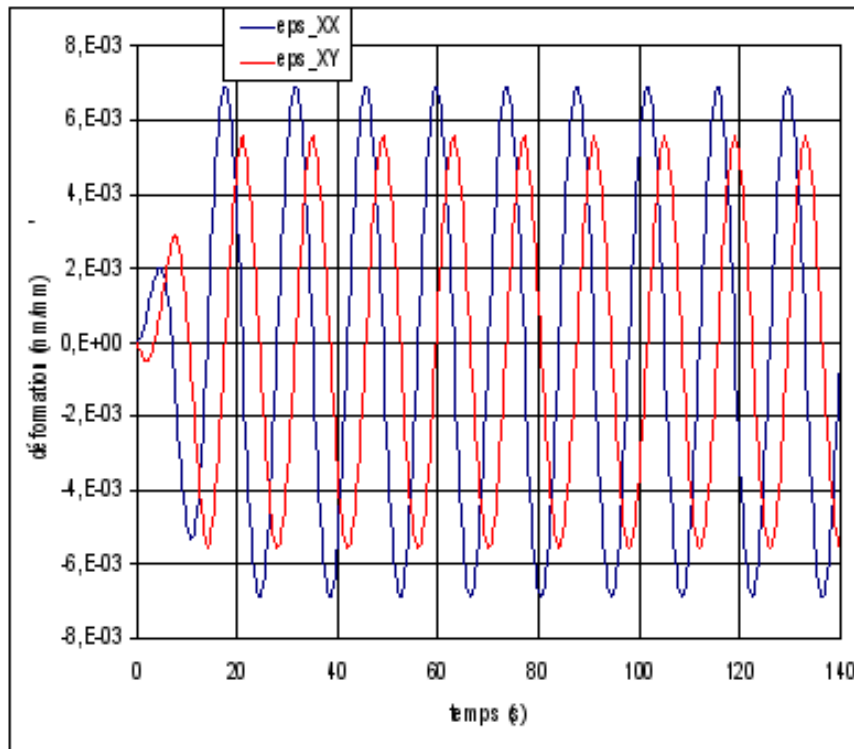
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# Problem to be solved

- ▶ The chosen model is suited to loading path ?
- ▶ What is the error in the integration of elastoplastic constitutive law ?
- ▶ How to avoid these errors?

# Problem to be solved

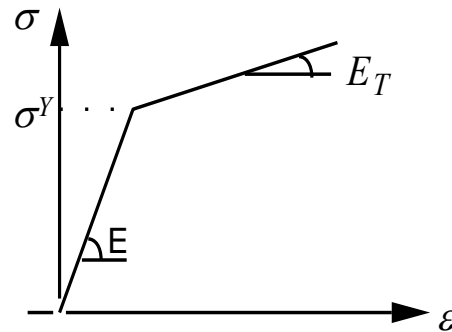
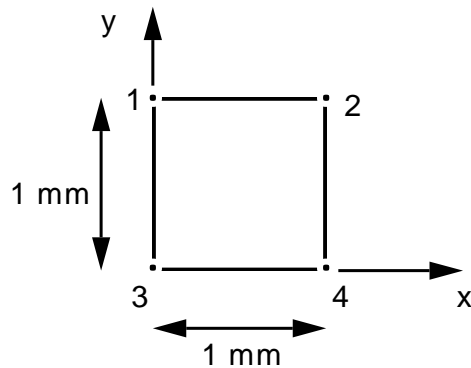
- ▶ Know the limitations of theoretical models used
  - Traction loading +  $90^\circ$  phase shifted torsion



# A (very) simple problem

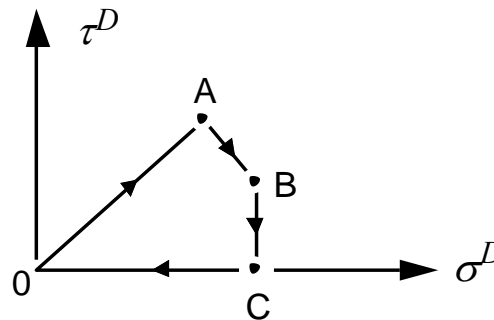
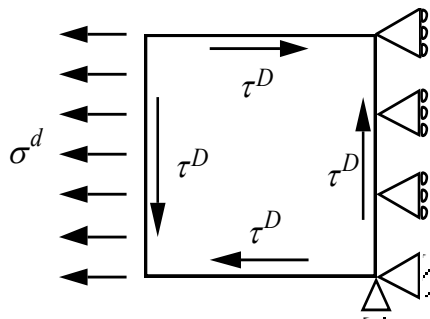
## ▶ Material point subjected to a loading path

### ■ Elastoplasticity with linear isotropic hardening



$E = 195000 \text{ MPa}$   
 $\nu = 0.3$   
 $\sigma^Y = 181 \text{ MPa}$   
 $E_T = 1930 \text{ MPa}$

### ■ Loading



	$\sigma^D$ (MPa)	$\tau^D$ (MPa)
A	151.2	93.1
B	257.2	33.1
C	259.3	0

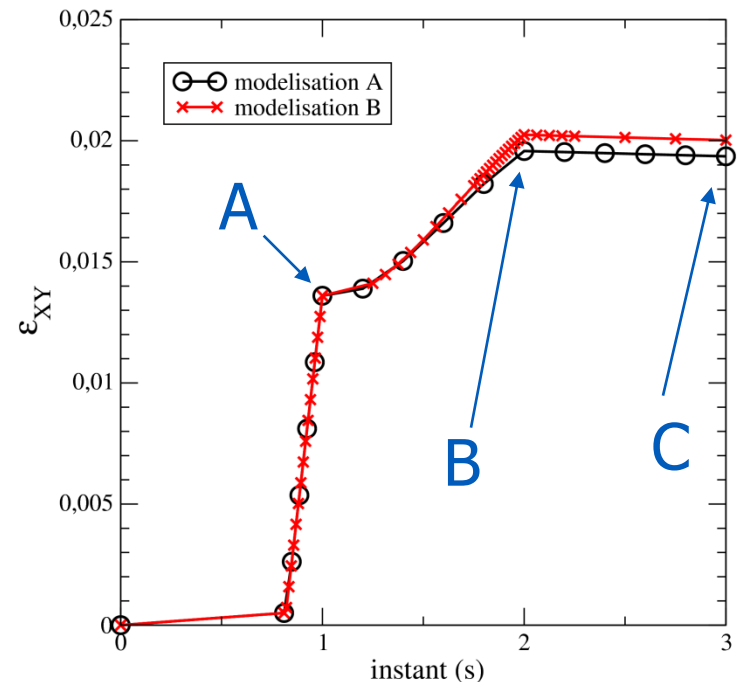
# Time discretization error

## 3 methods of resolution



- Analytical resolution -> reference values for  $\varepsilon_{xy}$
- Model A : coarse time discretization
- Model B : fine time discretization

(between two time steps, the cumulated plastic strain is constrained not to increase no more than  $0.1 \cdot 10^{-2}$ )

	Relative error of $\varepsilon_{XY}$	
Time step	Model A	Model B
1 s (point A)	0,003 %	0,003%
2 s (point B)	4,3%	1,1 %



# Implicit discretization

	Continuous	Discrete
Constitutive law	$\varepsilon(t) \rightarrow \sigma(t)$ $\begin{pmatrix} \varepsilon \\ \alpha \end{pmatrix} \xrightarrow{\dot{\varepsilon}} \dot{\alpha}$ $\sigma = \sigma(\varepsilon, \alpha)$	$\varepsilon(t_i) = \varepsilon_i \rightarrow \sigma(t_i) = \sigma_i$ $\begin{pmatrix} \varepsilon_i \\ \alpha_i \end{pmatrix} \xrightarrow{\Delta \varepsilon} \Delta \alpha$ $\sigma_{i+1} = \sigma(\varepsilon_{i+1}, \alpha_{i+1}, \varepsilon_i, \alpha_i)$
		 <b>Choice of the scheme</b>
Isotropic hardening + implicit scheme	$1) \sigma = A : (\varepsilon - \varepsilon^p) \quad R = R(p)$ $2) \dot{\varepsilon}^p = \frac{3}{2} \dot{\lambda} \frac{\tilde{\sigma}}{\sigma_{eq}} \quad \dot{p} = \dot{\lambda}$ $3) \dot{\lambda} f = 0 \quad \dot{\lambda} \geq 0 \quad f \leq 0$	$1) \sigma^+ = A : (\varepsilon^+ - \varepsilon^{p+}) \quad R^+ = R(p^+)$ $2) \frac{\Delta \varepsilon^p}{\Delta t} = \frac{3}{2} \frac{\Delta \lambda}{\Delta t} \frac{\tilde{\sigma}^+}{\sigma_{eq}^+} \quad \frac{\Delta p}{\Delta t} = \frac{\Delta \lambda}{\Delta t}$ $3) \Delta \lambda f^+ = 0 \quad \Delta \lambda \geq 0 \quad f^+ \leq 0$
		 <b>Implicit order 1 scheme</b>

# Error

▶ 1

$$\Delta p = \int_{t^-}^{t^+} \frac{dp}{dt} dt = \int_{\lambda^-}^{\lambda^+} d\lambda = \Delta\lambda$$

OK

▶ 2

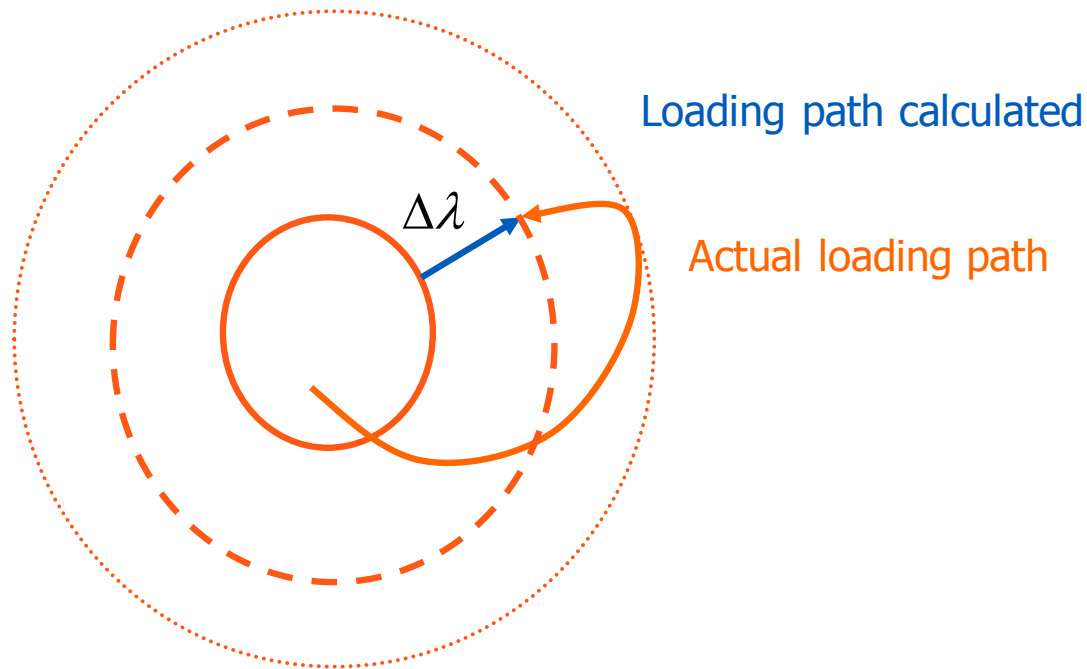
$$\Delta \varepsilon^p = \int_{t^-}^{t^+} \frac{d\varepsilon^p}{dt} dt = \int_{t^-}^{t^+} \frac{d\lambda}{dt} n(\lambda) dt = \int_{\lambda^-}^{\lambda^+} n(\lambda) d\lambda$$

$$\approx \int_{\lambda^-}^{\lambda^+} \left[ n(\lambda^+) + n'(\lambda^+) \cdot (\lambda - \lambda^+) \right] d\lambda = n(\lambda^+) \Delta\lambda - n'(\lambda^+) \cdot \frac{\Delta\lambda^2}{2}$$

**Error!**

# Error

- ▶ 3 : if  $\dot{\lambda} \geq 0$   $f \leq 0$  from  $t^-$  to  $t^+$  : OK, except if : load + undload in 1 single time step.





# Error

- ▶ Main source of error : 
$$-n'(\lambda^+). \frac{\Delta\lambda^2}{2}$$
- ▶ Exact integration
  - Permanent load during the loading step
  - The normal to the criterion is not reversing ("radial" load )
- ▶ Refine the time step outside these two cases!
- ▶ But how to detect?

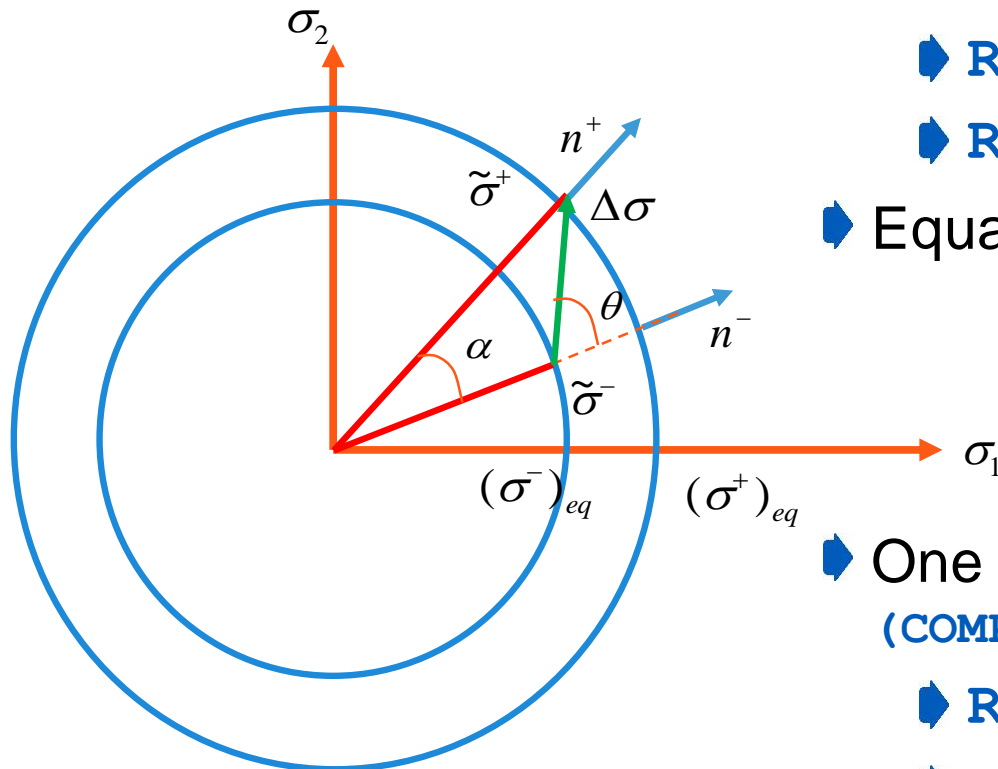
# Evaluation of the error

► Relative error on integration :

$$\eta = \frac{\|\delta\Delta\varepsilon^p\|}{\|\Delta\varepsilon^p\|} = \frac{\|n'(\lambda)\| \frac{\Delta\lambda^2}{2}}{\|n(\lambda)\| \Delta\lambda} = \frac{\|n'(\lambda)\| \frac{\Delta\lambda}{2}}{1}$$
$$\approx \left\| \frac{\Delta n}{\Delta\lambda} \right\| \frac{\Delta\lambda}{2} = \frac{1}{2} \|\Delta n(\lambda)\|$$

# An indicator of loss of "radiality"

$$\eta = \frac{1}{2} \|\Delta n\| = \left| \sin \frac{\alpha}{2} \right| \approx \frac{|\sin \theta|}{2}$$



The error is measured  
by  $\alpha$  and  $\theta$

▶ One define **DERA\_ELGA** (**CALC\_CHAMP**)

▶ **RADI\_T** =  $\left| \sin \frac{\alpha}{2} \right|$

▶ **RADI\_V** =  $(1 - \cos \theta)$

▶ Equals 0 when the loading is radial

▶ One define **RESI\_RADI\_RELA**  
(**COMP\_INCR**)

▶ **RADI\_T**

▶ **VMIS\_xx**

# Sufficient conditions of radiality

- ▶ "Radiality" = when the threshold normal is not reversing

$$\sigma(x,t) = \alpha(t) \sigma_0(x)$$

- ▶ Radiality conditions

- External loads are proportional
- Initial state undeformed and not hardened
- Von Mises plasticity with isotropic hardening  $R(p) = Cp^n$

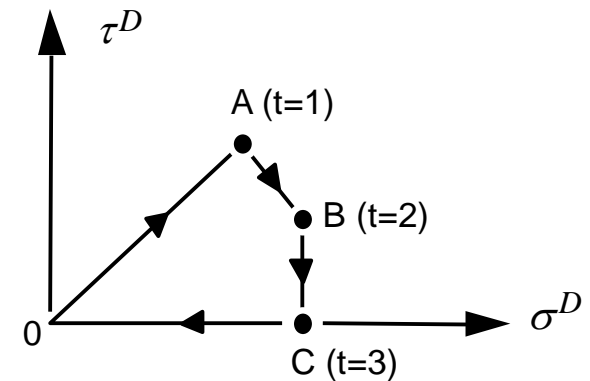
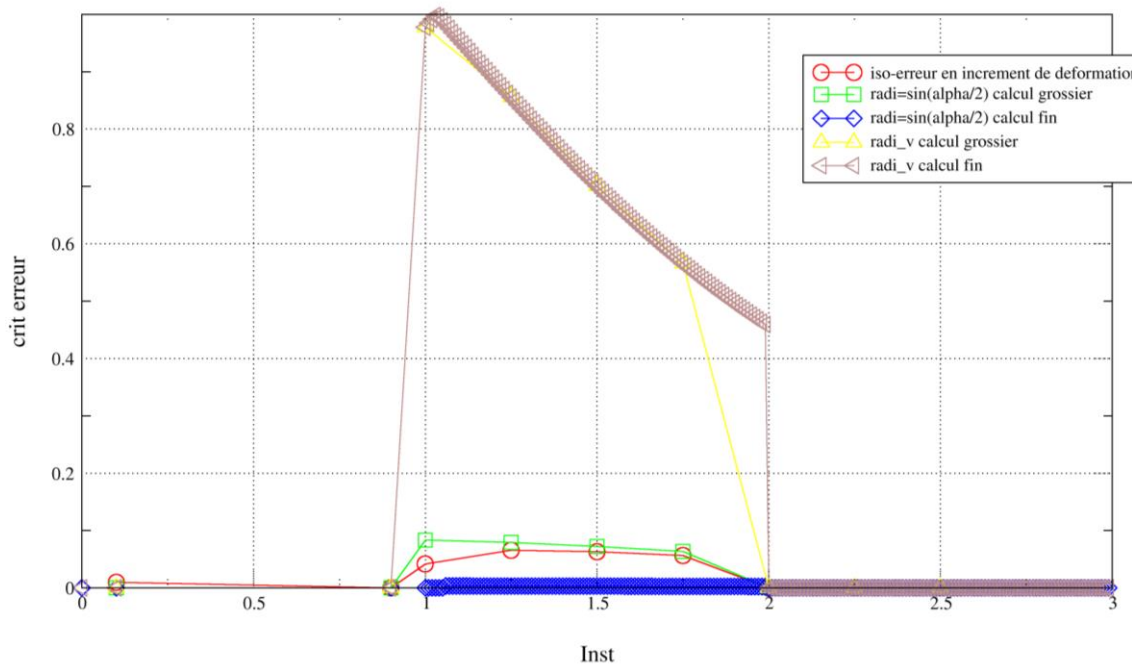
- ▶ Advantages

- Exact local integration
- Easy global convergence

- ▶ In the other cases, refine the time step !

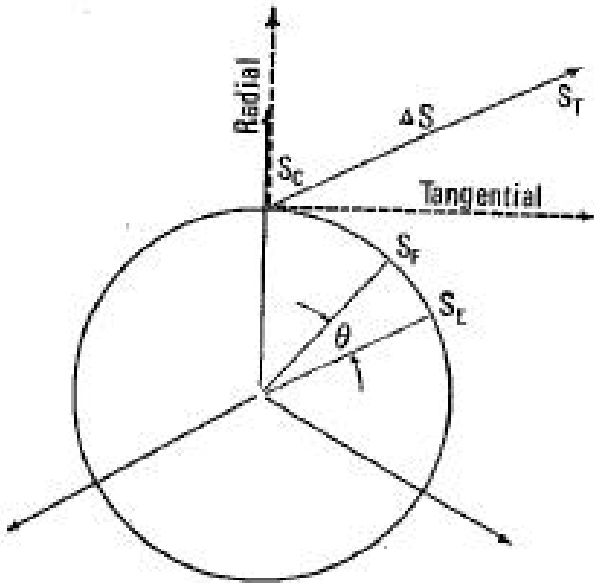
# practical example : TP1

- ▶ Indicator of radiality : **DERA\_ELGA** in **CALC\_CHAMP**
- ▶ Component(s): **RADI\_T** or **RADI\_V**

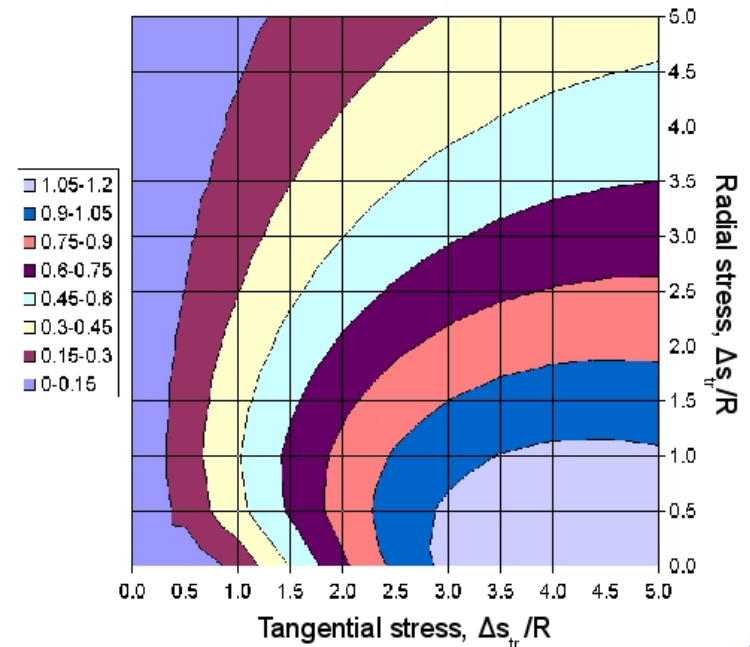
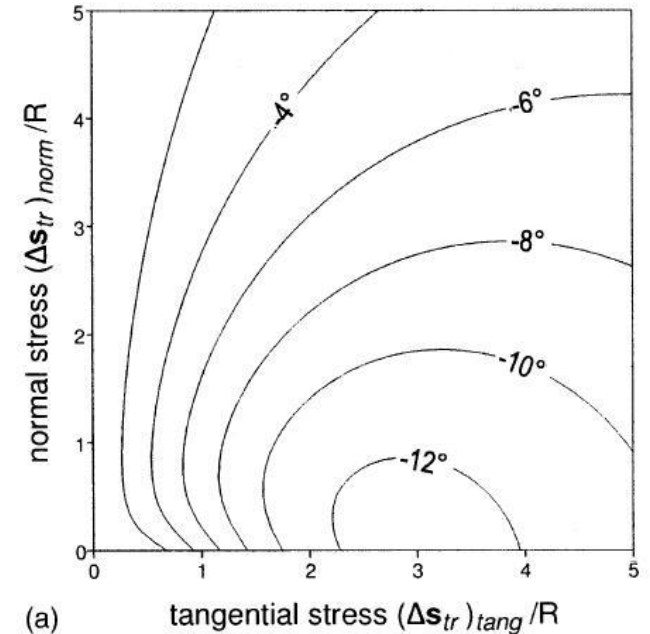


# Example taken from literature

► Perfect Von-Mises elasto-plasticity



$$ERR = \frac{\sqrt{(\sigma_n - \sigma_{ex}) : (\sigma_n - \sigma_{ex})}}{\sqrt{\sigma_{ex} : \sigma_{ex}}} \times 100\%$$



# End of presentation

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Or feeling happy to have read such a clear tutorial?

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