
Operator DEFI_MATER_GC

1 Goal

The operator `DEFI_MATER_GC` allows to define the material parameters used for studies of civil engineer.

The objective is to help the user to define the parameters materials starting from more physical size.

In this order, the physical properties are informed (elastic, yield stress coefficients, characteristic resistances,...), at exit one has a concept material, which one can then assign to the various meshes with the order `AFFE_MATERIAU`.

Product a structure of data of the type `to subdue`.

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2 General syntax

```
to subdue [to subdue] = DEFI_MATER_GC (
  ◇ INFORMATION = /1 [Defect]
    /2
  ◇/ MAZARS = _F (
    ◇ CODING = ['BAEL91', 'EC2', 'TEST'] [Text]

    # if CODING = 'BAEL91'
    ◇ UNITE_CONTRAINTTE = ['Mpa' | ' Pa'] [Text]
    ◇ FCJ = fcj [Reality]

    # if CODING = 'EC2'
    ◇ UNITE_CONTRAINTTE = ['Mpa' | ' Pa'] [Text]
    ◇ CLASS = ['C12/15' | ' C16/20' | ' C20/25' |
               'C25/30' | ' C30/37' | ' C35/45' |
               'C40/50' | ' C45/55' | ' C50/60' |
               'C55/67' | ' C60/75' | ' C70/85' |
               'C80/95' | ' C90/105'] [Text]

    # if CODING = 'TEST'
    ◇ FCJ = fcj [Reality]
    ◇ EIJ = eij [Reality]
    ◇ EPSI_C = epsi_c [Reality]
    ◇ FTJ = ftj [Reality]
    ◇ NAKED = naked [Reality]
    ◇ EPSD0 = epsid0 [Reality]
    ◇ K = K [Reality]
    ◇ AC = ac [Reality]
    ◇ BC = bc [Reality]
    ◇ AT = At [Reality]
    ◇ BT = BT [Reality]
    # For postprocessing
    ◇ SIGM_LIM = sigmlim [Reality]
    ◇ EPSI_LIM = epsilim [Reality]
  )

  ◇/ BETON_GLRC = _F (
    ◇ CODING = ['EC2', 'TEST'] [Text]

    # if CODING = 'EC2'
    ◇ UNITE_CONTRAINTTE = ['Mpa' | ' Pa'] [Text]
    ◇ CLASS = ['C12/15' | ' C16/20' | ' C20/25' |
               'C25/30' | ' C30/37' | ' C35/45' |
               'C40/50' | ' C45/55' | ' C50/60' |
               'C55/67' | ' C60/75' | ' C70/85' |
               'C80/95' | ' C90/105'] [Text]

    # if CODING = 'TEST'
    ◇ FCJ = fcj [Reality]
    ◇ EIJ = eij [Reality]
    ◇ EPSI_C = epsi_c [Reality]
    ◇ FTJ = ftj [Reality]
    ◇ NAKED = /naked [Reality]
    / 0.2 [DEFECT]
  )
)
```

```
♦/ENDO_FISS_EXP = _F (
  ♦ E = E [Reality]
  ♦ NAKED = naked [Reality]
  ♦ FT = ft [Reality]
  ♦ FC = FC [Reality]
  ♦ GF = Gf [Reality]
  ♦/P = p [Reality]
  /G_INIT = Ginit [Reality]
  ♦/Q = Q [Reality]
  /Q_REL = q_rel [Reality]
  ♦ LARG_BANDE = dble_D [Reality]
  ♦ COEF_RIGI_MINI = Rmin [Reality]
  ♦ REST_RIGI_FC = rrc [Reality]
)

♦/ENDO_LOCA_EXP = _F (
  ♦ E = E [Reality]
  ♦ NAKED = naked [Reality]
  ♦ FT = ft [Reality]
  ♦ FC = FC [Reality]
  ♦ GF = Gf [Reality]
  ♦ P = p [Reality]
  ♦ DIST_CRACK = Lf [Reality]
  ♦ REST_RIGI_FC = rrc [Reality]
)

♦/STEEL = _F (
  ♦ E = Young [Reality]
  ♦ SY = sigy [Reality]
  ♦ NAKED = naked [Reality]
  ♦ D_SIGM_EPSI = dsde [Reality]
  # For postprocessing
  ♦ SIGM_LIM = sigmlim [Reality]
  ♦ EPSI_LIM = epsilim [Reality]
)

♦ RHO = rho [Reality]
♦ ALPHA = appha [Reality]
♦ AMOR_ALPHA = will amora [Reality]
♦ AMOR_BETA = amorb [Reality]
♦ AMOR_HYST = amorh [Reality]
)
```

3 Order DEFI_MATER_GC

3.1 Objective of the order

The order DEFI_MATER_GC aims to simplify the entry of the coefficients materials for an application to the civil engineer, with the following laws:

- concrete law MAZARS,
- law of concrete for GLRC_DM,
- steel law ECRO_LINE,
- law of damage nonlocal of the concrete ENDO_FISS_EXP,
- law of damage local of the concrete ENDO_LOCA_EXP.

In this order, the physical properties are informed (elastic, yield stress coefficients, characteristic resistances,...), at exit one lays out of a concept "material", which one can then assign to the various meshes with the order AFFE_MATERIAU.

These concepts "material" at exit can also be used by the operator DEFI_GLRC, for the cases concrete armed for GLRC_DM and steel ECRO_LINE.

3.2 Operand INFORMATION

Allows to have, in the file of message, the echo of the order DEFI_MATERIAU used by DEFI_MATER_GC at the time of the definition of material.

The order DEFI_MATER_GC always print the parameters of material which are transmitted to the order DEFI_MATERIAU (confer the paragraph "example of use").

3.3 Other operands

Operands RHO, ALPHA, AMOR_ALPHA, AMOR_BETA, AMOR_HYST correspond and have the same meaning as those which one finds under the key word factor ELAS order DEFI_MATERIAU [U4.43.01].

4 Key word factor MAZARS

The model of behavior of Mazars is an elastic model of behavior endommageable making it possible to describe the softening behavior of the concrete. It distinguishes behaviour in traction and compression.

4.1 Operand CODING

The order DEFI_MATER_GC can use code of practice or advices resulting from codings to determine the parameters of the law of behavior MAZARS.

- ◆ CODING = 'BAEL91' | ' EC2' | ' ESSAI'
- 'BAEL91' : indicate that the parameters used in the definition of materials result from coding BAEI 1991 .
- 'EC2' : indicate that the parameters used in the definition of materials result from coding EUROCODE 2 .
- 'TEST' : indicate that the parameters used in the definition of materials come from test.

For example, according to BAEI 1991, for the material concrete knowing its characteristic resistance in compression FCJ , its resistance in traction can be estimated by: $FTJ=0.6+0.06FCJ$ where FTJ and FCJ are in MPa .

4.1.1 Case where CODIFICATION=' BAEI91'

The parameters used in the definition of materials result from coding BAEI 1991.

◆ UNITE_CONTRAINTE

Unit of constraint of the problem [MPa | Pa]: Méga-Pascal or Pascal. The seizure of this operand is obligatory, because the formulas used in the continuation requires to know if the parameters materials are in Pa or MPa . Lbe parameters materials which are returned by the order are in the same system of unit. UNITE_CONTRAINTE must thus be compatible with the units of the study.

- Pa : the parameters materials are homogeneous with Pa .
- MPa : parameters materials are homogeneous with MPa .

◆ FCJ

Constraint with the peak in compression, in Pa or MPa , according to the value of UNITE_CONTRAINTE.

4.1.2 Case where CODIFICATION=' EC2'

◆ UNITE_CONTRAINTE

Unit of constraint of the problem MPa or Pa : Méga-Pascal or Pascal. The seizure of this operand is obligatory, because it is necessary to turn over the parameters materials in the system of unit used to make the study.

◆ CLASS

Resistance in compression of the concrete is indicated by strength classes related to the characteristic resistance measured on cylinder or cube, in accordance with IN 206-1 .

The classes available in the operator are all those defined in EUROCODE 2 :

'C12/15' 'C16/20' 'C20/25' 'C25/30' 'C30/37' 'C35/45' 'C40/50'
'C45/55' 'C50/60' 'C55/67' 'C60/75' 'C70/85' 'C80/95' 'C90/105'

4.1.3 Case where CODIFICATION=' ESSAI '

In this case, the user must inform all the characteristics necessary to determine the parameters of the law of behavior of MAZARS. The user must give these characteristics in a system of units compatible with his study.

Obligatory parameters:

- ◆ FCJ : Constraint with the peak in compression.
- ◆ EIJ : Young modulus.
- ◆ EPSI_C : Deformation with the peak in compression.
- ◆ FTJ : Constraint with the peak in traction.

Optional parameters, presented in the table 4.1.3-a, are those which one finds under the key word factor MAZARS order DEFI_MATERIAU [U4.43.01].

EPSD0	Threshold of damage in deformation
AC , B C	Coefficients allowing to fix the pace of the curved post-peak in compression.
AT , B T	Coefficients allowing to fix the pace of the curved post-peak in traction.
K	Parameter of correction for shearing.

Table 4.1.3-a : Parameters materials of law MAZARS.

- ◆ NAKED : Poisson's ratio.
- ◆ SIGM_LIM : Ultimate stress.
- ◆ EPSI_LIM : Limiting deformation.

4.2 Operation

4.2.1 Parameters of the law MAZARS

The parameters of the law are given using the following characteristics: FCJ, EIJ, EPSI_C, FTJ. The formulas are:

$$\varepsilon_0 = f_{ij} / E_{ij} \quad \beta = 1.10 \quad B_T = E_{ij} / f_{ij} \quad A_T = 0.70$$

$$B_c = \frac{1}{\varepsilon_c \nu \sqrt{2}} \quad A_c = \frac{\left(\frac{f_{cj} \nu \sqrt{2}}{E_{ij}} - \varepsilon_0 \right)}{\varepsilon_c \nu \sqrt{2} \% \exp \left(B_c (\varepsilon_0 - \varepsilon_c \nu \sqrt{2}) \right) - \varepsilon_0}$$

$$\sigma_{ELS} = 0.6 f_{cj} \quad \varepsilon_{ELU} = 3.5 \text{‰}$$

A_c and B_c are given by solving the equations resulting from the writing 1D behavior of MAZARS in order to respect the constraint and the deformation with the peak, as well as the horizontal tangent with the peak.

- B_c is obtained while solving $f'(\varepsilon_c) = 0$
- A_c while solving $f_{cj} = f(\varepsilon_c)$.

4.2.2 In the case BAEL 1991

Two operands are obligatory: UNITE_CONTAINTE, FCJ.

The order determines the sizes necessary by formulas or rules resulting from BAEL91. In the formulas below Lbe sizes f_{cj}, f_{ij}, E_{ij} are in MPa .

$$E_{ij} = 11000.0 \sqrt[3]{f_{cj}} \quad f_{ij} = 0.6 + 0.06 f_{cj} \quad \varepsilon_c = 0.620E-3 \sqrt[3]{f_{cj}} \quad \nu = 0.200$$

Parameters of the law of MAZARS are then given.

4.2.3 In the case EUROCODE 2

Two operands are obligatory: UNITE_CONTAINTE, CLASS.

The order determines the sizes necessary by formulas or rules resulting from EUROCODE 2. In the formulas below $f_{ck}, f_{cm}, f_{ctm}, E_{cm}$ are in MPa.

f_{ck} : characteristic resistance in compression measured on cylinder to 28 days.

f_{cm} : average resistance in compression of the concrete to 28 days.

$$f_{cm} = f_{ck} + 8.0$$

f_{ctm} : average resistance in traction of the concrete.

$$f_{ctm} = \begin{cases} 0.30 f_{ck}^{2/3} & \text{pour classe} \leq C50/60 \\ 2.12 \log(1 + f_{cm}/10) & \text{pour classe} > C50/60 \end{cases}$$

E_{cm} : tangent module

$$E_{cm} = 22.0E+03 \left(\frac{f_{cm}}{10} \right)^{0.3}$$

ε_{c1} : deformation with the peak in ‰

$$\varepsilon_{c1} = 0.7 f_{cm}^{0.31} \text{ toujours } \leq 2.8$$

ε_{cu1} : ultimate limiting deformation in ‰ .

$$\varepsilon_{cu1} = \begin{cases} 2.80 + 27 \left[\frac{98 - f_{cm}}{100} \right]^4 & \text{pour classe} > C50/60 \\ 3.5 & \text{pour classe} \leq C50/60 \end{cases}$$

Parameters of the law of MAZARS are then given.

4.2.4 In the case TEST

Four operands are obligatory : FCJ, EIJ, EPSI_C, FTJ. Parameters of the law of behavior of MAZARS are given like previously.

So operands optional presented to the table 4.1.3-a are informed, they are taken into account by the order. It is thus necessary to make sure of the coherence of the provided sizes, in particular in the following cases:

- the user gives B_c . The equation $f'(\varepsilon_c) = 0$ can not be checked, in this case the behavior will pass by the point f_{cj} but f_{cj}, ε_c will not be any more a extremum.
- the user gives A_c . The equation $f_{cj} = f(\varepsilon_c)$ can not be checked, in this case the behavior will not pass by the point f_{cj} and ε_c .

4.3 Example of use

To define a concrete which has a behavior of MAZARS with a resistance characteristic of 40.0 MPa for a study whose constraints must be in Pa, the order is used in the following way:

```
BETONM = DEFI_MATER_GC (  
    MAZARS = _F (FCJ=40.0E+06, UNITE_CONTRAINTE = "Phas", ) ,  
)
```


The order prints in the file of message all the values which are used to define material.

```

== PARAMÈTRES OF LAW MAZARS [PA] ==
ELASTICITY PART:
  E = 3.76194246E+10, NAKED = 2.00000000E-01,
NON-LINEAR PART:
  BT = 1.25398082E+04, K = 0.70000000E+00,
  AT = 7.00000000E-01, EPSI_LIM = 3.50000000E-03,
  BC = 1.66741558E+03, SIGM_LIM = 2.40000000E+07,
  AC = 1.28292129E+00, EPSD0 = 7.97460364E-05,
FOR INFORMATION:
  FCJ = 4.000E+07, FTJ = 3.0000E+06, EPSI_C = 2.12036757E-03,
    
```

The table 4.3-a give sets of parameters obtained with the rules previously described.

F_{cj} [MPa]	30,0	35,0	40,0	45,0	50,0
F_{tj} [MPa]	2,4	2,7	3,0	3,3	3,6
Young [MPa]	34180,0	35982,0	37619,0	39126,0	40524,0
Nu	0,2	0,2	0,2	0,2	0,2
$Epsi_c$	1,93E-03	2,03E-03	2,12E-03	2,21E-03	2,28E-03
At	0,7	0,7	0,7	0,7	0,7
Bt	14241,0	13327,0	125 39. 8	11856,0	11257,0
$Epsi0$	7,02E-05	7,50E-05	7.9 7 E-05	8,43E-05	8,88E-05
Bc	1835,2	1743,3	1667,4	1603,2	1547,9
Ac	1,128	1,209	1,283	1,351	1,415

Table 4.3-a : Parameters for the law MAZARS.

The figure 4.3-a present the various curves of compression obtained with the values of the table 4.3-a.

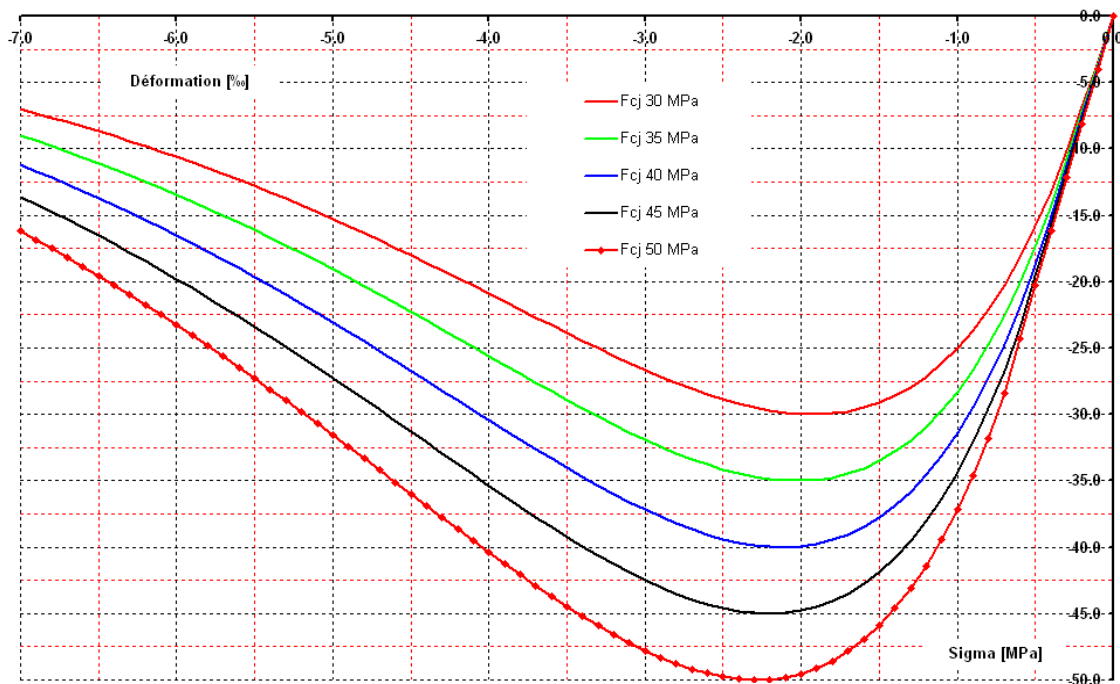


Figure 4.3-a : Law of MAZARS curves of compression $\sigma = f(\epsilon)$.

5 Key word factor `BETON_GLRC`

This keyword factor is used to define concrete material which will be provided to the keyword `BETON/MATER` of `DEFI_GLRC/RELATION=' GLRC_DM'`.

5.1 Operand CODING

This operand functions in the same way as that of the keyword `MAZARS`.

- ◆ `CODING = 'EC2' | 'ESSAI'`
- `'EC2'` : indicate that the parameters used in the definition of materials result from coding EUROCODE 2 .
- `'TEST'` : indicate that the parameters used in the definition of materials come from test.

5.1.1 Case where `CODIFICATION=' EC2 '`

◆ `UNITE_CONTRAINTE`

Unit of constraint of the problem *MPa* or *Pa* : Méga-Pascal or Pascal. The seizure of this operand is obligatory, because it is necessary to turn over the parameters materials in the system of unit used to make the study.

◆ `CLASS`

Resistance in compression of the concrete is indicated by strength classes related to the characteristic resistance measured on cylinder or cube, in accordance with `IN 206-1` .

The classes available in the operator are all those defined in `EUROCODE 2` :

`'C12/15' 'C16/20' 'C20/25' 'C25/30' 'C30/37' 'C35/45' 'C40/50'`
`'C45/55' 'C50/60' 'C55/67' 'C60/75' 'C70/85' 'C80/95' 'C90/105'`

5.1.2 Case where `CODIFICATION=' ESSAI '`

In this case, the user must inform the following parameters which will be formatted in a concept "material" in order to be with the format expected by `DEFI_GLRC`. The user must give these characteristics in a system of units compatible with his study.

- ◆ `FCJ` : Constraint with the peak in compression.
- ◆ `EIJ` : Young modulus.
- ◆ `EPSI_C` : Deformation with the peak in compression.
- ◆ `FTJ` : Constraint with the peak in traction.
- ◇ `NAKED` : Poisson's ratio. (0.2 by defaults)

6 Key word factor STEEL

The model of behavior is elastoplastic with a linear kinematic work hardening.

6.1 Operands

Operands are those which one finds under words keys factors ELAS and ECRO_LINE order DEFI_MATERIAU [U4.43.01].

- ◆ E : Young, elastic slope modulus of the curve $\sigma = f(\varepsilon)$
- ◆ SY : Elastic limit.

- ◇ NAKED : Poisson's ratio
- ◇ D_SIGM_EPSI : Slope of work hardening on the curve $\sigma = f(\varepsilon)$. (cf . ECRO_LINE order DEFI_MATERIAU).

- ◇ SIGM_LIM : Ultimate stress.
- ◇ EPSI_LIM : Limiting deformation.

6.2 Operation

Two operands are obligatory: E, SY. So operands optional are indicated, they are taken into account by the order and the values will not be modified. It is thus necessary to make sure of the coherence of the provided sizes.

If operands optional are not indicated, the order determines them missing sizes by the following formulas:

$$\nu = 0.3 \quad dsde = E / 10000.0 \quad \sigma_{ELS} = \sigma_y / 1.1 \quad \varepsilon_{ELU} = 10.0\%$$

6.3 Examples of use

To define a steel with a yield stress of 400.0MPa , the order is used in the following way:

```
STEEL = DEFI_MATER_GC (  
    STEEL = _F (E=2.0E+11, SY=400.0E+06, ) ,  
)
```

The order prints in the file of message all the values which are used to define material.

```
== PARAMÈTRES OF LAW ECRO_LINE ==  
ELASTICITY PART:  
E = 2.000E+11, NAKED = 3.00000000E-01,  
NON-LINEAR PART:  
SY = 4.00000000E+08, EPSI_LIM = 1.00000000E-02,  
D_SIGM_EPSI = 2.00000000E+07, SIGM_LIM = 3.63636364E+08,  
FOR INFORMATION:  
EPSI_ELAS = 2.00000000E-03,
```

7 Key word factor ENDO_FISS_EXP

The model of behavior `ENDO_FISS_EXP` of behavior endommageable is an elastic model not room (available in modeling `GRAD_VARI`). It makes it possible to describe the softening behavior of the concrete. It distinguishes in particular behaviour in traction and in compression, partially rigidity in compression restores and described well the states of shearing or bi-traction. When the characteristic length tends towards zero, it approaches a cohesive model, which explains why one informs parameters characteristic of a cohesive law more than of a voluminal model of damage.

7.1 Operands

E	Young modulus (Pa)
NAKED	Poisson's ratio
FT	Threshold of damage in simple traction (Pa)
FC	Threshold of damage in compression (Pa)
GF	Energy of cracking (N/m)
P	Parameter of principal work hardening of the asymptotic cohesive law
G_INIT	Energy of partial cracking resulting from the initial slope
Q	Secondary parameter of work hardening of the asymptotic cohesive law
Q_REL	Secondary parameter of work hardening (ranging between 0 and 1)
LARG_BANDE	Bandwidth of localization (m)
REST_RIGI_FC	Coefficient of restoration of rigidity (0 = without restoration)
COEF_RIGI_MINI	Threshold of swing to the fixed secant tangent matrix

Table 7.1-a : Parameters materials of law `ENDO_FISS_EXP`

7.2 Operation

Certain characteristics do not require complementary explanations: the Young modulus, the Poisson's ratio, thresholds of damage in traction and compression, the energy of cracking. They are usual characteristics for the modeling of the damage of the concrete.

Concerning the parameters `P` and `Q` who characterize the standardized answer of the asymptotic cohesive model (the constraint is standardized by `FT`, the opening by `GF/FT`), one places at the disposal several manners to inform them. One can directly inform `P` (superior with 1) or the effect of `P` on the initial slope of the cohesive answer via the data of the energy of corresponding cracking `G_INIT` if the model of cohesive softening were linear with like slope the initial slope. This manner of characterizing the initial slope is used by certain authors, in particular within the framework of a bilinear cohesive law (one speaks then about `GF`, with tiny, in opposition to `GF`, with a capital letter, which indicates the entirety of the energy of cracking). For `Q`, one can directly inform his value (worthless by default) but this one is obligation to remain between 0 and one value maximum which depends on `P`. to simplify the data of `Q`, one gives the opportunity of informing `Q` into relative compared to this maximum value via the keyword `Q_REL` (with value between 0 and 1, therefore).

Concerning the restoration of rigidity, the model `ENDO_FISS_EXP` introduced a parameter of regularization `Y` who smoothes the jump of rigidity between traction and compression. Rather than to inform the value directly of `Y`, not necessarily very speaking, one prefers to indicate via `REST_RIGI_FC` the level of rigidity restored compared to initial rigidity for a deformation (in compression) equalizes with `FC/E`. This value thus lies between 0 (no restoration of rigidity) and 1 (strictly lower than 1, total restoration of rigidity not being possible with the function of selected regularization). A value of 0.9 by default is proposed.

One introduces finally the bandwidth of localization which is supposed to reflect a cohesive crack. It is the double of the parameter `D` (which measures him to it half-width of band in `1D`, as described in the theoretical reference of the model).

As for the parameter `COEF_RIGI_MINI`, it is that introduced into `DEFI_MATERIAU` [U4.43.01]. When the residual rigidity standardized by `E` is lower than `COEF_RIGI_MINI`, one substitutes for the tangent matrix the secant matrix corresponding to this rigidity, which limits the problems involved in possible completely destroyed zones (i.e without residual rigidity). This parameter is without incidence on the physique of the model, it intervenes only on the properties of convergence of the algorithm of Newton. By default, this function is not activated (`COEF_RIGI_MINI = 0`), which seems very well to be appropriate in most case.

In a general way, one returns to the reference material of the model [R5.03.28] for more detailed explanations on the significance of the various parameters of the model.

8 Key word factor ENDO_LOCA_EXP

The model of behavior ENDO_LOCA_EXP of elastic behavior endommageable is a model local. It makes it possible to describe the softening behavior of the concrete. It distinguishes in particular behaviour in traction and in compression, partially rigidity in compression restores and described well the states of shearing or bi-traction. From its local character, it is dedicated to a homogenized representation of the structural cracks, which explains the introduction of a distance inter-crack which fixes the size of the zones containing at more the one crack. At the level of this zone, its answer is close to that of ENDO_FISS_EXP who, would describe the detail of the crack to him. Certain parameters are thus common with those of ENDO_FISS_EXP. For more information, one will be able to refer to the document [R7.01.42] and the references which are quoted there.

8.1 Operands

E	Young modulus (Pa)
NAKED	Poisson's ratio
FT	Resistance in simple traction (Pa)
FC	Resistance in compression simple (Pa)
GF	Energy of cracking (N/m)
P	Parameter of work hardening
DIST_CRACK	Average distance inter-crack (m)
REST_RIGI_FC	Coefficient of restoration of rigidity (0 = without restoration)

Table 8.1-a : Parameters materials of law ENDO_LOCA_EXP

8.2 Operation

Certain characteristics do not require complementary explanations: the Young modulus, the Poisson's ratio, them resistances in traction and compression, the energy of cracking. They are usual characteristics for the modeling of the damage of the concrete.

The parameter P influence the form of work hardening, leading to an answer stress-strain all the more curved since it is large. It is similar to the parameter P law ENDO_FISS_EXP . There is not another parameter characterizing work hardening: compared to ENDO_FISS_EXP , one chose to take Q=0 .

Concerning the restoration of rigidity, the model ENDO_LOCA_EXP introduced a parameter of regularization γ who smoothes the jump of rigidity between traction and compression. Rather than to inform the value directly of γ , not necessarily very speaking, one prefers to indicate via REST_RIGI_FC the level of rigidity restored compared to initial rigidity for a deformation (in compression) equalizes with FC/E. This value thus lies between 0 (no restoration of rigidity) and 1 (strictly lower than 1, total restoration of rigidity not being possible with the function of selected regularization). A value of 0.9 is proposed by default.

One introduces finally DIST_FISSURE average distance inter-crack, which depends in particular on the reinforcements in the concrete. In practice, only the ratio GF/DIST_FISSURE play a part but one preferred to preserve the two parameters because each one carries a specific physical significance. For reasons of local stability of the model (not of snap-back at the level of the material point), there exists a limit upper than the distance inter-crack than one can model. The respect of this condition is controlled at the time of the setting in data.