

## SSNV228 – Setting in pre-tensioning of a Summarized

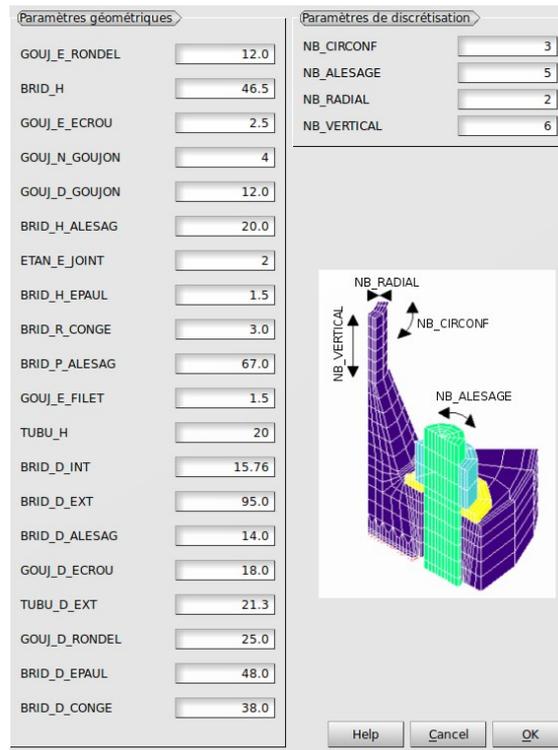
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### **pin:**

This test illustrates the setting in pre-tensioning of a pin in Code\_Aster. Methodology selected consists in applying a relative displacement between a group of elements of the pin and a group of elements of the nut (between the two sides which are normally threaded). Two modelizations are proposed:

- Modelization a: manual determination of displacement.
- Modelization b: determination automated of displacement using `MACR_RECAL`.

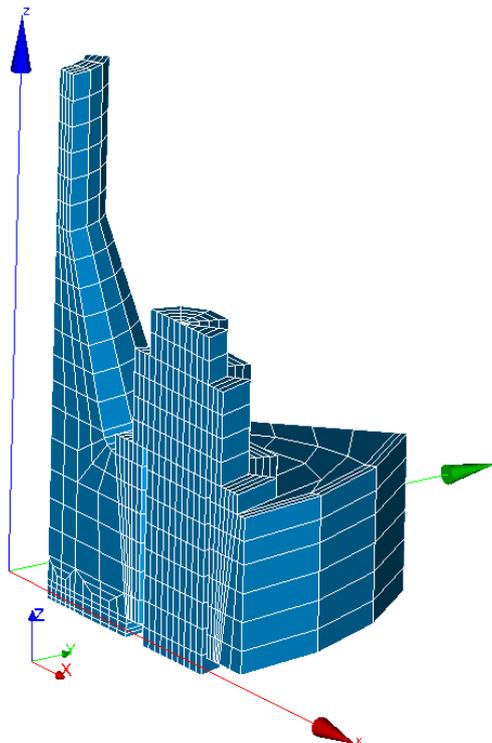




Appear1.2-b

## 1.3 Mesh

The mesh, presented to the figure1.3-a, is also generated by the dedicated tools “Computation of flange” of SALOME-MECA-2012.1. It linear and is composed of 1108 hexahedrons and 70 prisms for 1821 nodes.



Appear :

## 1.4 Materials

the material is elastic and its properties are:  $E = 200\,000\text{ MPa}$  and  $\nu = 0.3$ .

## 1.5 Boundary conditions, of contact and loading

the boundary conditions of blockings are the following ones:

- blocking of the degree of freedom  $DZ$  on the sides of the lower part of the pin and the joint,
- conditions of symmetry via the blocking of the normal displacement of the side face with boring,
- conditions of symmetry via the blocking of the normal displacement of the side face without boring,
- condition of flatness of the face of cut of the tube in the plane  $XY$  by imposing a value identical for the degree of freedom  $DZ$  to all the nodes of the face,
- condition of tightening via a difference null between the  $DX$  degrees of freedom and  $DY$  of the nodes of the nut and of the pin in opposite,
- pressure of  $1.0\text{E-}06\text{ Pa}$  inside the tube.
- condition of contact between the sides of the joint and the flange.

The loading corresponds to a relative displacement imposed on the nodes of the nut and pin. It is null at time zero and is worth  $DEPL\_R$  at time  $1.0$ .

### Note:

Displacement is named  $DEPL\_R$  so as to A re-use the command file of the modelization directly with  $MACR\_RECAL$  in the modelization B. Indeed, the macro-command requires the presence of "" at the end of the name of the parameters to be readjusted.

## 1.6 Modelization

The modelization is 3D.

## 1.7 Required force

One seeks to apply a displacement  $DEPL\_R$  corresponding to a average constraint of  $30\text{ MPa}$  in the rod of the pin, that is to say a force resulting from:

$$F^{\text{résultant}} = \sigma^{\text{pré-tension}} \cdot \pi \cdot R_{\text{goujon}}^2 / 2 = 1695.6\text{N} . \text{ Division by 2 takes account of symmetry.}$$

## 2 Modelization A

### 2.1 Characteristic of the modelization

This modelization illustrates the methodology of tightening of a pin. It is a question of imposing a relative displacement between the nodes of the nut and the pin and of calculating the resulting force. The computation is realized by modifying the value of `DEPL_R` until the resulting force corresponds to the required force.

### 2.2 Quantities tested and results

retiming carried out is considered to be satisfactory when `DEPL_R` is of  $8.0E-3\text{ mm}$ . This value makes it possible to put the pin in pre-tensioning with a average constraint of  $30\text{ MPa}$  in the rod of the pin.

The resulting force is compared to the required force.

Result	Reference	Value of reference	Tolerance
Force resulting on nut	ANALYTIQUE	-1695.6 N	1.0E-02

From the tests of NON-regression with a tolerance from  $1.0E-6$  are carried out on the forces resulting from the following sides:

- face of the nut in contact with the pin,
- face of the pin in contact with the nut,
- face of the lower part of the pin,
- face of the joint in contact with the flange,
- face of the flange in contact with the joint.

*Note: the resulting force calculated on each side is identical.*

## 3 Modelization B

### 3.1 Characteristic of the modelization

This modelization illustrates the methodology of the setting in tension of a pin by carrying out an automatic retiming of the value of relative displacement between the nodes of the nut and the pin. For that, one uses macro-command `MACR_RECAL` in a master file and the modelization A like slave file.

The function of the force targets to reach:

```
CIBLE=DEFI_FONCTION (
  NOM_PARA=' INST',
  NOM_RESU=' DZ',
  VALE= ( 0.0 , 0.0 ,
         1.0 , F_RESULT, ),
)
```

the call to the ordering of retiming:

```
RECAL=MACR_RECAL (
  PARA_OPTI = _F (NOM_PARA=' DEPL_R ',
                 VALE_INI=0.004, VALE_MIN=0.004, VALE_MAX=0.012, ),
  COURBE    = _F (FONC_EXP=CIBLE, NOM_FONC_CALC=' REACF',
                 PARA_X=' INST', PARA_Y=' DZ'),
)
```

In slave file the computation of `REACF` :

```
REACF=POST_RELEVE_T (
  ACTION=_F (INTITULE=' FZ_CEG',
            OPERATION=' EXTRACTION',
            RESULTAT=RESU,
            NOM_CHAM=' REAC_NODA',
            RESULTANTE=' DZ',
            GROUP_NO=' N_SCEG', ),
)
```

### 3.2 Quantities tested and results

retiming carried out makes it possible to determine a value of `DEPL_R` close to  $8.0E-3 \text{ mm}$ . This value makes it possible to put the pin in tension with a average constraint of  $30 \text{ MPa}$  in its rod.

The only quantity which it is possible to recover in concept `MARC_RECAL` is the value of the parameter. THE `TEST_RESU` is thus carried out on this value, and it is a test of NON-regression.

Result	Reference	Value of reference	Tolerance
resulting Force on the nut	NOT REGRESSIO N	0.0079595	5.0E-06

*Note* : in slave file printing of `REACF` is carried out. The value of the force corresponding to the parameter is  $-1.69560E+03$ , which corresponds to the value of the target force.

## 4 Summary of the results

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the two methods make it possible to obtain the same one result, that is to say a relative displacement to force near to  $8.0E-3 \text{ mm}$  obtain a average constraint of  $30 \text{ MPa}$  in the pin.