

## HPLV102 - Computation of $G$ thermoelastic in infinite medium for a circular crack

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### Abstract

It acts of a test of fracture mechanics into thermomechanical for an axisymmetric problem. One considers a circular crack plunged in a presumedly infinite medium. One imposes a uniform temperature on the lips of crack. This test makes it possible to calculate rate of energy restitution  $G$ .

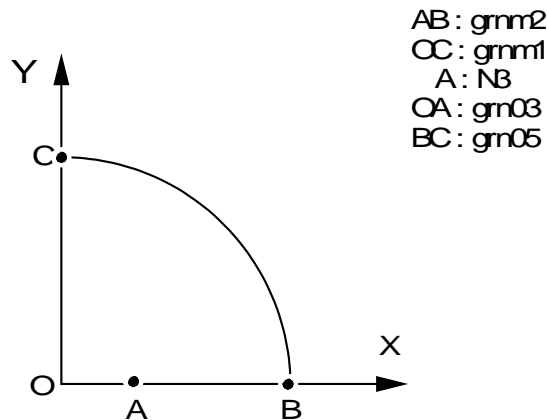
The interest of the test is the stability of  $G$  according to various contours and the comparison with an analytical solution.

This test contains a modelization into axisymmetric.

The variations of the computation of  $G$  on various contours compared to the reference solution do not exceed 1,5%.

## 1 Problem of reference

### 1.1 Geometry



It acts of a circular crack of radius  $OA=5$  .

The presumedly infinite medium is modelled by a sphere of radius  $OB=600$  .

### 1.2 Material properties

thermal Conductivity:	$\lambda=1.$
Thermal coefficient of thermal expansion:	$\alpha=10^{-6}/^{\circ}C$
Young modulus:	$E=2.10^5 MPa$
Poisson's ratio:	$\nu=0.3$

### 1.3 Boundary conditions and loadings

- Mechanics: Displacement imposed

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(GROUP_NO: grnm1 DX: 0.)
(GROUP_NO: grnm2 DY: 0.)
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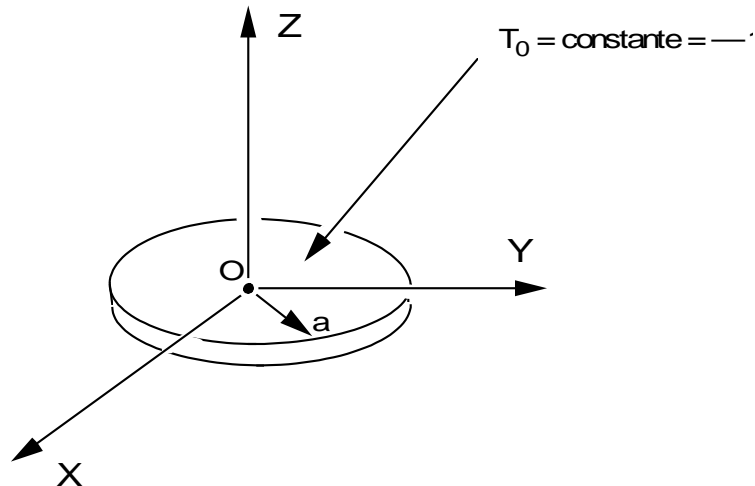
- Thermal: TEMP\_IMPO

```
(GROUP_NO: grno3 TEMP: 0. )
(GROUP_NO: grno5 TEMP: -1.)
(THE NODE IS OUTSIDE THE FIELD OF DEFINITION WITH A
RIGHT PROFILE OF THE EXCLU TYPE NODE:      N3
TEMP: -1.)
```

## 2 Reference solution

### 2.1 Method of calculating used for the reference solution

the reference solution is resulting from OLESIAK and SNEDDON [bib1]:



The statement of the rate of refund of energy is the following one:

$$G = \frac{(1-\nu^2)}{E} K_1^2 \quad \text{with} \quad K_1 = \frac{\alpha E}{\Pi(1-\nu)} T_0 \sqrt{\Pi a}$$

$$\text{is: } G = \frac{(1-\nu^2)}{\Pi(1-\nu)^2} \alpha^2 E T_0^2 a$$

### 2.2 Result of reference

result of reference is thus:  $G = 5.9115 \cdot 10^{-7} \text{ J/m}^2$

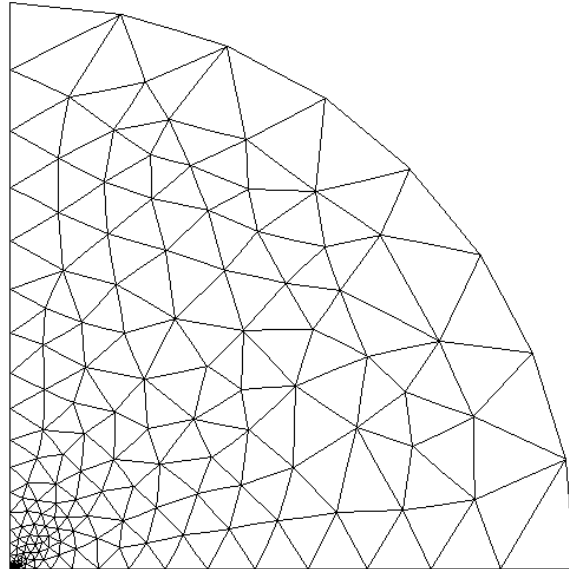
### 2.3 Bibliographical reference

- 1) Uniform Temperature one has Penny-Shaped Ace (OLESIAK and SNEDDON (1959)), included in Handbook of stress-intensity, factors of G.C. SIH.

## 3 Modelization A

### 3.1 Characteristic of the modelization

It acts of a modelization into axisymmetric:



### 3.2 Characteristics of the mesh

Many nodes: 832

Number of meshes and types: 323 TRIA6, 42 QUAD8, 59 SEG3

Crown 1:	$R_{inf} = 1.$	$R_{sup} = 4.$
Crown 2:	$R_{inf} = 0.5$	$R_{sup} = 4.5$
Crown 3:	$R_{inf} = 1.5$	$R_{sup} = 3.5$
Crown 4:	$R_{inf} = 1.$	$R_{sup} = 4.5$

### 3.3 Quantities tested and results of the modelization A

the values tested are those of the rate of refund of energy  $G$  on various integration contours:

Identification	Reference	Aster	% Tolerance
Crowns 1 $G$	$1.4778 \cdot 10^{-6}$	$1.4586 \cdot 10^{-6}$	1.50
Contour 2 $G$	$1.4778 \cdot 10^{-6}$	$1.4574 \cdot 10^{-6}$	1.50
Contour 3 $G$	$1.4778 \cdot 10^{-6}$	$1.4583 \cdot 10^{-6}$	1.50
Contour 4 $G$	$1.4778 \cdot 10^{-6}$	$1.4573 \cdot 10^{-6}$	1.50

## 3.4 Notices

the value of reference is  $G = 5.945 \cdot 10^{-7} \text{ J/m}^2$

It is given per unit of area of extension of crack, therefore for  $a=5$  and taking into account the symmetry of the mesh, it is necessary to compare result Aster with:  $G_{Aster} = G_{réf} \times \frac{a}{2} = 1.4778 \cdot 10^{-6}$ , because it  $G$  in Aster to a surface of extension of 1 radian corresponds.

## 4 Summary of the Invariance

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results of result compared to contours. Correct thermal term.