

---

---

## HSLV304 - Roll under thermal loading

---

---

### Abstract:

The goal of the test is to validate a decomposable thermal loading in 2 harmonics, applied to an axisymmetric structure (cylinder in fact).

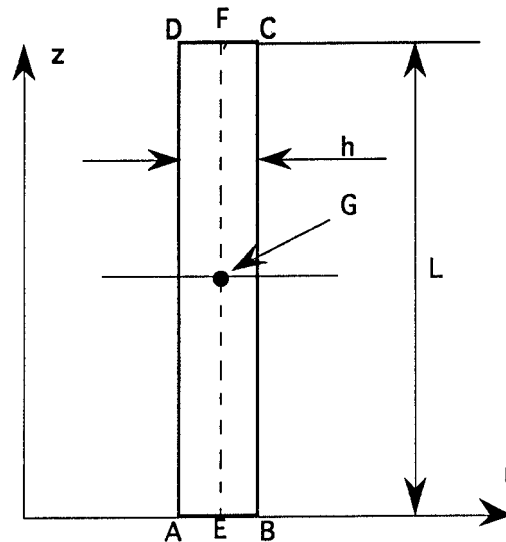
The harmonies considered are harmonies 1 and 2.

The comparison is carried out compared to a model shell, with a software finite elements.

In the modelization  $B$ , one imposes a strain field  $\varepsilon_0$  defined by `AFFE_CHAR_MECA`, corresponding to the strain field from the model  $A$ . The goal is to compare the results compared to those obtained for the model  $A$ .

## 1 Problem of reference

### 1.1 Geometry



Length	: $L=4\text{ m}$	Position of the points $E, F, G$
Thickness	: $H=0,1\text{ m}$	• $E, F, G$ remotely $R_0$ of the axis
Average radius	: $R_0=1\text{ m}$	• $G$ with middle height

### 1.2 Material properties

$$E=2.1 \times 10^{11} \text{ Pa}$$
$$\nu=0.3$$
$$\alpha=0.12 \times 10^{-4} / ^\circ \text{C}$$

### 1.3 Boundary conditions and loadings

- Sections  $AB$  and  $CD$  clamped
- Field of temperature  $T = \cos \theta + \sin 2\theta$

### 1.4 Initial conditions

Without object for the static analysis.

## 2 Reference solution

---

### 2.1 Method of calculating used for the reference solution

Comparison of the results compared to the software finite elements CASTOR-SD of CETIM.

The element of BEAVER used is an isoparametric shell element with 8 nodes, based on the formulation of Ahmad. It is about a degenerated three-dimensional element, whose scope of application is that of the thick shells.

### 2.2 Results of reference

- Displacement and stresses with the points  $E, F, G$  for each harmonic.
- Displacement and stresses at the points  $E, F, G$  for the total loading.

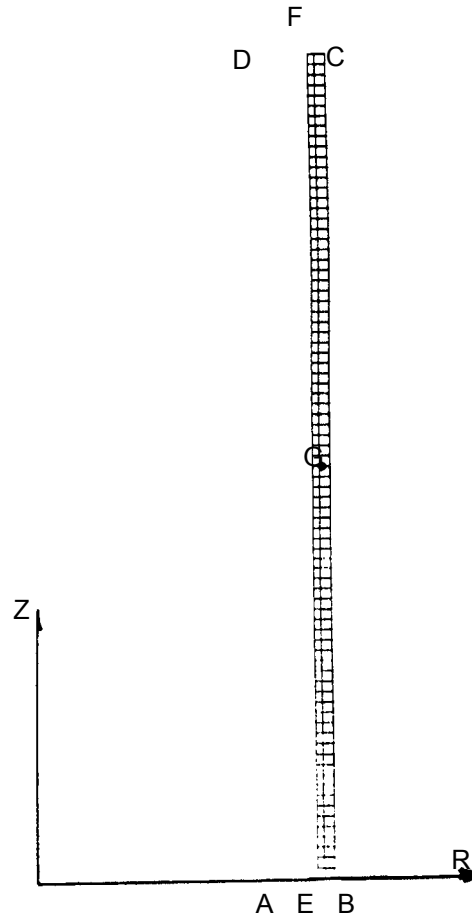
### 2.3 Uncertainty on the solution

Comparison of software.

## 3 Modelization A

### 3.1 Characteristic of the modelization

Modelization AXIS\_FOURIER, meshes QUAD8



uniform

Loading Field of temperatures  $T_0=1$  .

Cutting: 80 elements according to the length  
2 elements according to the radius

Name of the nodes:

$A=N1$   $B=N2$   $C=N3$   $D=N4$   $E=N9$   $F=N171$   $G=N71$

### 3.2 Characteristics of the mesh

Many nodes: 645

Number of meshes and types: 160 QUAD8

## 3.3 Quantities tested and Standard

	Localization	results of Standard	value of Reference	Values of reference	% Tolerance
Charge in $\cos \theta$	Point $G$	$u_r(m)$	SOURCE EXTERNE	0.96 X 10-5	0.10
		$u_\theta(m)$		0.15 X 10-5	0.10
Load in $\sin 2 \theta$	Point $G$	$u_r(m)$	SOURCE EXTERNE	0.544426 X 10-5	0.10
Load total	Point $G$	$u_r(m)$	SOURCE EXTERNE	1.50748 10-5	0.10
		$u_\theta(m)$		1.52412 10-5	0.10

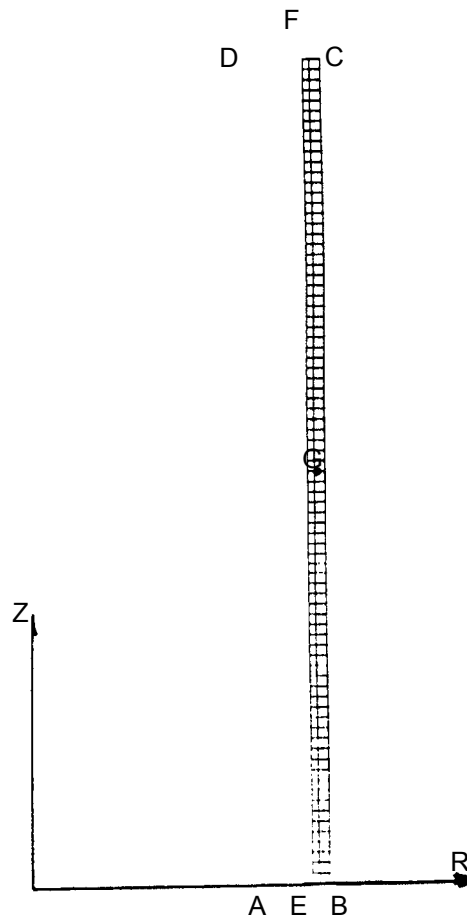
## 3.4 Remark

Models finite elements of reference: 640 shell elements with 8 nodes (10 elements according to the length – 64 elements according to the circumference).

## 4 Modelization B

### 4.1 Characteristic of the modelization

Modelization AXIS\_FOURIER, meshes QUAD8



Loading

Field of pre strains  $\varepsilon_0 \text{ constant} = \alpha T_0$   $T_0 = 1$  .

(  $\varepsilon_{rr} = \varepsilon_{zz} = \varepsilon_{\theta\theta} = 0.12 \times 10^{-4}$  )

Cutting: 80 elements according to the length  
2 elements according to the radius

Name of the nodes:

A=N1 B=N2 C=N3 D=N4 E=N9 F=N171 G=N371

### 4.2 Characteristics of the mesh

Many nodes: 645

Number of meshes and types: 160 QUAD8

## 4.3 Quantities tested and Standard

	Localization	results of Standard	value of Reference	Values of reference	% Tolerance
Charge in $\cos \theta$	Point $G$	$u_r(m)$	SOURCE EXTERNE	0.96 X 10-5	0.10
		$u_\theta(m)$		0.15 X 10-5	0.10
Load in $\sin 2 \theta$	Point $G$	$u_r(m)$	SOURCE EXTERNE	0.544426 X 10-5	0.10
Load total	Point $G$	$u_r(m)$	SOURCE EXTERNE	1.50748 10-5	0.10
		$u_\theta(m)$		1.52412 10-5	0.10

## 5 Summary of the results

---

the results got for the modelization  $B$  in which one imposes like predeformations the strains resulting from the modelization  $A$ , are identical to those of the modelization  $A$ .