

## SSNP302 - Element charged in thermics - Appearance of the secondary stresses

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### Summary:

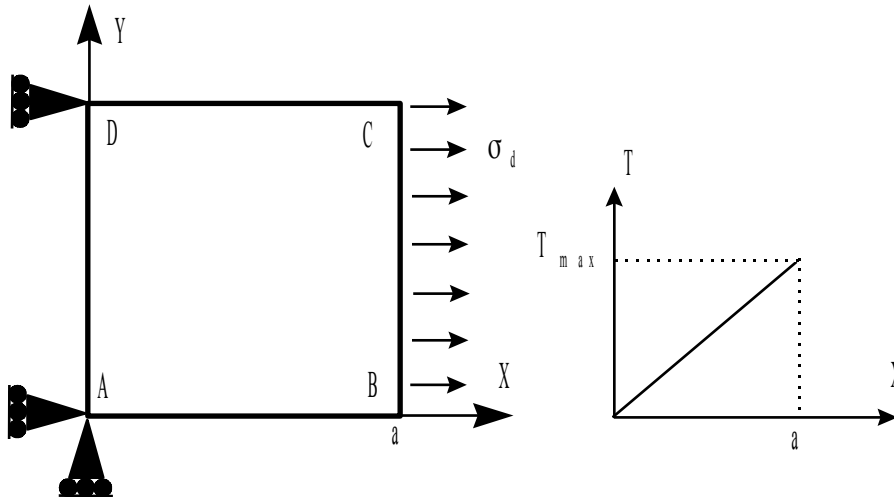
This test of linear quasi-static mechanics 2D consists in charging in thermics an element with plate to degree 1, by applying a field of temperature which varies linearly on the element and by fixing a side of the element.

This element being of degree 1, the total mechanical deformation will be constant in the element. The fields thermics imposing a linear deformation in the element, it will be necessary to take a dilation coefficient and a sufficiently large heat gradient to make the deformation mechanical total sensitive to the imposed thermal field.

The plate is modelled by an element plan (MECPQU4).

## 1 Problem of reference

### 1.1 Geometry



Length  $a=1$

### 1.2 Material properties

Isotropic elastic material:

$$E = 200000 \text{ Mpa}$$

$$\nu = 0.$$

$$\alpha = 1\text{E-}6 / ^\circ\text{C}$$

### 1.3 Boundary conditions and loadings

Not  $A$  :  $u_x = 0.$

$$u_y = 0.$$

On the side  $AD$  :  $u_x = 0.$

On the side  $BC$  :  $\sigma_D = 100 \text{ MPa}$

Application of a field of temperature which varies linearly on the element with  $T_{max} = 1000^\circ\text{C}.$

## 2 Reference solution

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### 2.1 Method of calculating used for the reference solution

Analytical solution.

### 2.2 Results of reference

The mechanical deformation is worth:

$$\begin{aligned}\varepsilon^{mec} &= \varepsilon - \varepsilon^{th} \\ &= \varepsilon - \alpha T\end{aligned}$$

With an element with the degree one and a diagram  $2 \times 2$  of integration one will have:

$$\begin{aligned}\varepsilon^{mec} &= \frac{u_{xB} - u_{xA}}{a} - \alpha \left[ \frac{1+\xi}{2} T_{max} \right] \\ &= \frac{\sigma_d}{E} + \frac{1}{2} \alpha T_{max} - \alpha \left[ \frac{1+\xi}{2} T_{max} \right]\end{aligned}$$

The constraint in the test will be worth:

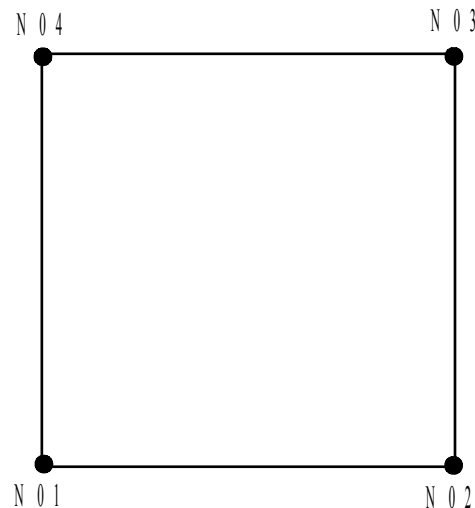
$$\sigma = E \varepsilon^{mec} \text{ with } \varepsilon^{mec} = 10^{-3} - \alpha \left[ \frac{1+\xi}{2} T_{max} \right]$$

### 2.3 Notice

The thermal component of the constraint depending on the intrinsic coordinate, the solution is to consider an average temperature by element.

## 3 Modeling A

### 3.1 Characteristics of modeling A



Modeling in plane constraints: C\_PLAN

The loading and the boundary conditions are modelled by:

- DDL\_IMPO (Node *NO1*  $DX=0$   
 $DY=0$  )  
(Node *NO4*  $DX=0$  )
- nodal forces imposed on the nodes *NO2* and *NO3*
- temperatures imposed on the nodes  
*NO1* , *NO4* :  $T=0^\circ$   
*NO2* , *NO3* :  $T=1000^\circ$

### 3.2 Characteristics of the grid

Many nodes: 4

Many meshes and types: 1 MECPQU4 with diagram of integration  $2 \times 2$

### 3.3 Sizes tested and results

Identification	Reference
<i>SIXX</i> ( <i>NO1</i> )	200
<i>SIXX</i> ( <i>NO4</i> )	200
<i>SIXX</i> ( <i>NO2</i> )	0
<i>SIXX</i> ( <i>NO3</i> )	0

# Code Aster

Version  
default

Titre : SSNP302 - Élément chargé en thermique - Apparition[...]  
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## 4 Summary of the results

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The results provided by Code\_Aster are very satisfactory.