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## WTNV135 - Triaxial compression test drained with model LETK of the CIH

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### Summary

This test makes it possible to validate the model `LETK` within the framework of a hydraulic modeling. It is about a triaxial compression test in drained condition.

By reason of symmetry, one is interested only in the eighth of a sample subjected to a triaxial compression test. The level of containment is of  $5\text{ MPa}$ .

Modeling A: Integration of the model by an explicit diagram, with classical modeling.

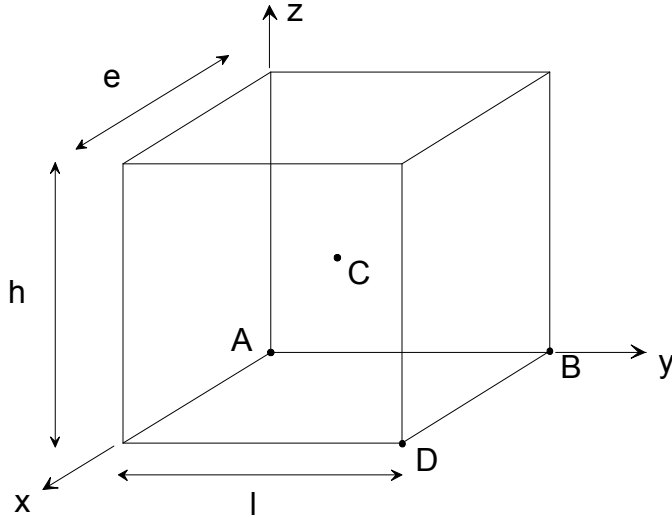
Modeling b: Integration of the model by implicit scheme whose matrix jacobienne is obtained by disturbance, with classical modeling.

Modeling C: Integration of the model by implicit scheme whose matrix jacobienne is obtained analytically, with classical modeling.

Modeling D: Integration of the model by an explicit diagram, with under-integrated modeling.

## 1 Problem of reference

### 1.1 Geometry



hauteur :  $h = 1 \text{ m}$   
largeur :  $l = 1 \text{ m}$   
épaisseur :  $e = 1 \text{ m}$

Coordinates of the points (in meters):

	A	B	C	D
x	0.	0.	0.5	1.
y	0.	1.	0.5	1.
z	0.	0.	0.5	0.

## 1.2 Material property

$$E = 5000 \text{ MPa}$$

$$\nu = 0.12$$

$$\alpha = 0.$$

$$Pa = 0.1 \text{ MPa}$$

$$n_{elas} = 0.$$

$$\sigma_c = 12. \text{ MPa}$$

$$H_0^{ext} = 1.10292$$

$$\gamma_{cjs} = 0.8$$

$$x_{ams} = 0,1$$

$$\eta = 0.04$$

$$a_0 = 0.25$$

$$a_e = 0.60$$

$$a_{pic} = 0.40$$

$$s_0 = 0.0005$$

$$m_0 = 0.01$$

$$m_e = 2.$$

$$m_{pic} = 6.$$

$$m_{ult} = 0.61$$

$$\xi_{ult} = 0.365$$

$$\xi_e = 0.028$$

$$\xi_{pic} = 0.015$$

$$m_{v-max} = 3.$$

$$\xi_{v-max} = 0.0039$$

$$A^v = 1.510^{-12} \text{ Pa}$$

$$n^v = 4.5$$

$$\sigma_{pl} = 57.8 \text{ MPa}$$

$$\mu_{0,v} = 0,1$$

$$\xi_{0,v} = 0,3$$

$$\mu_1 = 0,1$$

$$\xi_1 = 0,3$$

## 1.3 Initial conditions, boundary conditions, and loading

### Phase 1:

One brings the sample in a homogeneous state:  $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0$ , by imposing the corresponding confining pressure on the front, side right-hand side and higher faces. Displacements are blocked on the faces postpones ( $u_x = 0$ ), side left ( $u_y = 0$ ) and lower ( $u_z = 0$ ).

### Phase 2:

One maintains displacements blocked on the faces postpones ( $u_x = 0$ ), side left ( $u_y = 0$ ) and lower ( $u_z = 0$ ). On all the faces, the pressure of water is worthless.

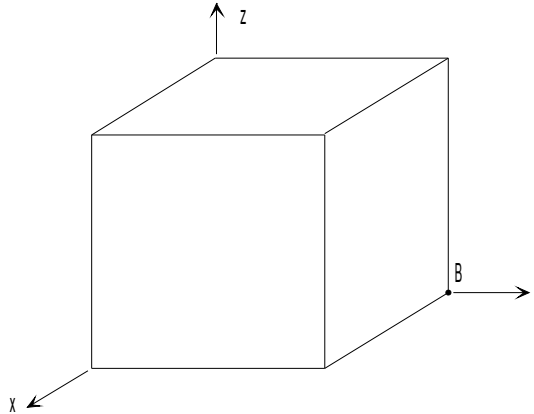
One applies a displacement forced to the higher face in order to obtain a deformation  $\varepsilon_{zz} = -6$  (counted starting from the beginning of phase 2). On the front faces and side right-hand side, one imposes a constraint of  $5 \text{ MPa}$ .

## 2 Reference solutions

The values of reference are obtained by not-regression. A finer discretization of the loading ensures the convergence of the values a limited value.

## 3 Modeling A

### 3.1 Characteristics of modeling



Cutting: 1 in height, in width and thickness.

Loading of phase 1:

Confining pressure:  $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0 : -5 \text{ MPa}$ .

Coefficient of biot: 1

UN\_SUR\_K water: 0

Modeling: 3D\_HM

### 3.2 Characteristics of the grid

Many nodes: 20

Many meshes and types: 1 HEXA20 and 6 QUA8

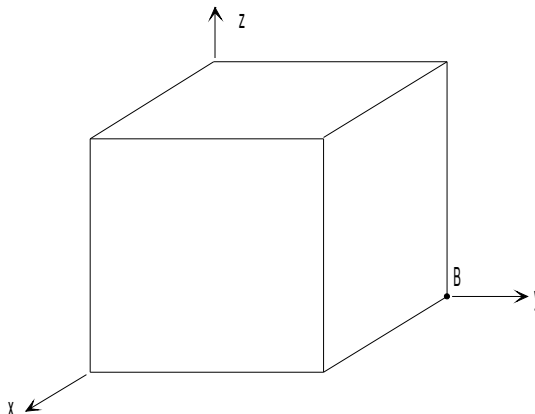
### 3.3 Sizes tested and results

The values are tested in not-regression with a precision given of 0,1 %

Localization	Moment	Displacement	Aster
Not C	13000.	$DX$	$3,019 \cdot 10^{-2}$
Localization	Moment	Constraint (MPa)	Aster
Not C	13000.	$\sigma_{zz}$	-11,941

## 4 Modeling B

### 4.1 Characteristics of modeling



Cutting: 1 in height, in width and thickness.

Loading of phase 1:

Confining pressure:  $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0 : -5 \text{ MPa}$ .

Coefficient of biot: 1

UN\_SUR\_K water: 0

Modeling: 3D\_HM

### 4.2 Characteristics of the grid

Many nodes: 20

Many meshes and types: 1 HEXA20 and 6 QUA8

### 4.3 Sizes tested and results

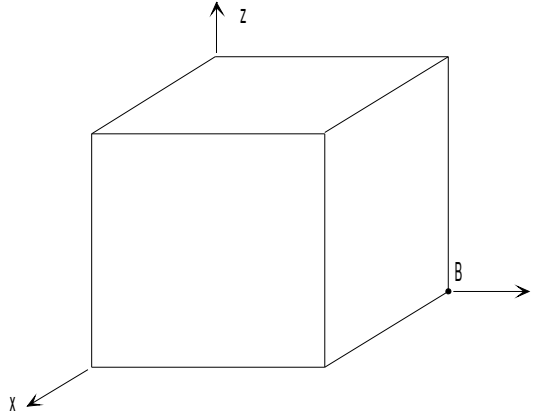
The values are tested in not-regression with a precision given of 0,1%

Localization	Moment	Displacement	Aster
Not C	13000.	$DX$	$3,026 \cdot 10^{-2}$

Localization	Moment	Constraint (MPa)	Aster
Not C	13000.	$\sigma_{zz}$	-11.94

## 5 Modeling C

### 5.1 Characteristics of modeling



Cutting: 1 in height, in width and thickness.

Loading of phase 1:

Confining pressure:  $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0 : -5 \text{ MPa}$ .

Coefficient of biot: 1

UN\_SUR\_K water: 0

Modeling: 3D\_HM

### 5.2 Characteristics of the grid

Many nodes: 20

Many meshes and types: 1 HEXA20 and 6 QUA8

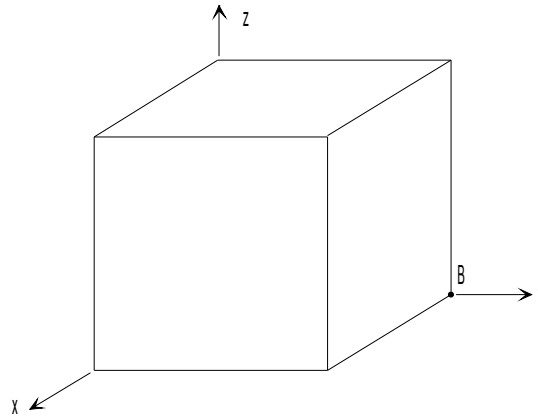
### 5.3 Sizes tested and results

The values are tested in not-regression with a precision given of 0,1%

Localization	Moment	Displacement	Aster
Not C	13000.	$DX$	$3,026 \cdot 10^{-2}$
Localization	Moment	Constraint (MPa)	Aster
Not C	13000.	$\sigma_{zz}$	-11.94

## 6 Modeling D

### 6.1 Characteristics of modeling



Cutting: 1 in height, in width and thickness.

Loading of phase 1:

Confining pressure:  $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0 : -5 \text{ MPa}$  .

Coefficient of biot: 1

UN\_SUR\_K water: 0

Modeling: 3D\_HM\_SI

### 6.2 Characteristics of the grid

Many nodes: 20

Many meshes and types: 1 HEXA20 and 6 QUA8

### 6.3 Sizes tested and results

The values are tested in not-regression with a precision given of 0,1%

Localization	Moment	Displacement	Aster
Not <i>C</i>	13000.	<i>DX</i>	3,019 10 <sup>-2</sup>
Localization	Moment	Constraint (MPa)	Aster
Not <i>C</i>	13000.	$\sigma_{zz}$	-11,941



## 7 Summary of the results

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This case test is a test of nonregression developed to validate the model `LETK` in hydromechanics in conditions drained for two distinct diagrams of integration. The results are identical to those obtained in test SSNV206 for the two diagrams.