

ZZZZ127 - Validation of the keyword LIAISON_MAIL

Summary:

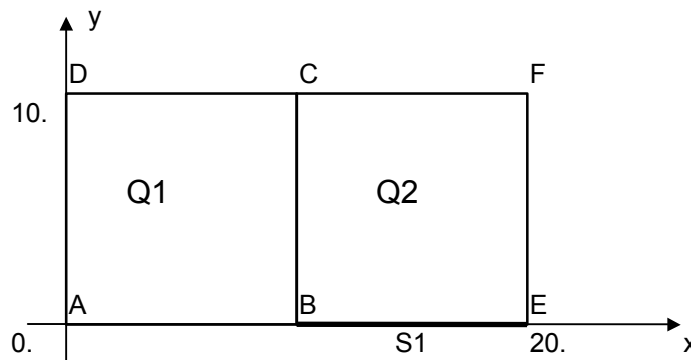
This test validates the keyword `LIAISON_MAIL` orders `AFPE_CHAR_MECA` and `AFPE_CHAR_THER`. This keyword generates the linear relations between the degrees of freedom of the nodes of 2 edges which one puts in opposite. The programming is validated in 2D and 3D by intercomparison with a calculation *Aster* similar where the relations between degrees of freedom directly entered by the keyword `LIAISON_DDL`. One also validates the geometrical transformation (rotation/translation) applied to the one of the edges.

1 Problem of reference

1.1 Geometry

With the dealt problem is plan. The studied structure is 1 rectangle cut out in 2 squares $ABCD$ and $BEFC$.

The solution is established with a network using 2 QUAD4 corresponding to the 2 squares.



1.2 Properties of material

elastic material:

$$E = 10.0 \quad \text{units S.I.}$$

$$\nu = 0.0$$

One takes $\nu = 0.0$ so that one can deal with this problem plan with a layer of elements 3D by having the plane solution.

1.3 Boundary conditions and loadings

1) One applies a specific force to the point F : $FY = 4.0$ u.s.i.

2) Blockings:

$$\text{not } A : DX = DY = 0.$$

$$\text{not } D : DX = 0.$$

3) Linear relations between degrees of freedom:

loading case: cas1

$$1.0 DX(E) - 0.5 DY(D) - 0.5 DY(C) = 0.0$$

$$1.0 DY(E) + 0.5 DX(D) + 0.5 DX(C) = 0.0$$

loading case: cas2

$$1.0 DY(E) + 0.5 DY(D) + 0.5 DY(C) = 0.0$$

$$1.0 DY(B) + 0.5 DY(C) + 0.5 DY(F) = 0.0$$

The initial conditions are of no importance here.

2 Reference solution

2.1 Method of calculating used for the reference solution

In each case, one carries out a preliminary calculation with the keyword `LIAISON_DDL` to introduce the linear relations between degrees of freedom. This calculation is used as reference to calculation with the keyword `LIAISON_MAIL` who generates these linear relations.

To obtain the desired linear relations with `LIAISON_MAIL`, one writes:

Cas1:

```
LIAISON_MAIL: ( NOEUD_2: E           MAILLE_1: Q1  
                CENTER: B           ANGL_NAUT: 90.   TRAN: (-5.  0.) )
```

What wants to say that one eliminates the 2 degrees of freedom from the node E according to the degrees of freedom of the point E' obtained when one subjects to E a rotation of 90 degrees around B then a translation of vector (-5.0) . E' is thus in the middle of CD . The vector displacement of E is identified (after rotation of 90 degrees) with that of E' . The 2 equations are thus obtained:

$$\begin{aligned}DX(E) &= DY(E') = 0.5 DY(C) + 0.5 DY(D) \\DY(E) &= -DX(E') = -0.5 DX(C) - 0.5 DX(D)\end{aligned}$$

Cas2:

```
LIAISON_MAIL: ( MAILLE_2: S1           MAILLE_1: (Q1, Q2)  
                DDL_2: 'DNOR'         DDL_1: 'DNOR'  
                CENTER: B           ANGL_NAUT: 180.  TRAN: (+5. +10.) )
```

What wants to say that one eliminates normal displacement from the nodes B and E (nodes of the segment SI) according to the degrees of freedom of the points B' and E' obtained when one subjects to B and E a rotation of 180 degrees around B then a translation of vector $(+5,+10)$. B' is thus in the middle of CF and E' in the middle of DC . The normal displacement of B is identified (after rotation of 180 degrees) with that of B' . One makes in the same way for E . The 2 equations then are obtained:

$$\begin{aligned}DY(E) &= -DY(E') = -0.5 DY(C) - 0.5 DY(D) \\DY(B) &= -DY(B') = -0.5 DY(C) - 0.5 DY(F)\end{aligned}$$

2.2 Results of reference

Displacement is observed DY point F :

$$\text{cas1: } DY(F) = 1.4153582447720D+00$$

$$\text{cas2: } DY(F) = 1.0561898652983D+00$$

These displacements are obtained with linear relations enter degrees of freedom introduced by the keyword `LIAISON_DDL`.

2.3 Uncertainties on the solution

Warning : The translation process used on this website is a "Machine Translation". It may be imprecise and inaccurate in whole or in part and is provided as a convenience.

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No uncertainty.

3 Modeling A

3.1 Characteristics of modeling

The problem is solved with modeling D_PLAN .

3.2 Characteristics of the grid

The grid is made of:

2 QUAD4: $Q1 = ABCD$ and $Q2 = BEFC$

1 SEG2: $SI = BE$

3.3 Sizes tested and results

Identification	Reference
cas1: $DY(F)$	1.4153582447720D+00
cas2: $DY(F)$	1.0561898652983D+00

4 Modeling B

4.1 Characteristics of modeling

The problem is solved with modeling 3D.

4.2 Characteristics of the grid

The grid is made of:

2 HEXA8: $Q1$ and $Q2$
1 QUAD4: SI

4.3 Features tested

The same ones as for modeling A but in 3D.

4.4 Sizes tested and results

Identification	Reference
cas1: $DY(F)$	1.4153582447720D+00
cas2: $DY(F)$	1.0561898652983D+00

5 Summary of the results

The digital results, displacement in a point, are rigorously identical between two calculations *Aster*, with the keyword `LIAISON_MAIL`, or with the keyword `LIAISON_DDL`.