

ZZZZ298 – Data-processing validation of POST_K1_K2_K3

Summary:

The purpose of this test is to validate in an elementary way the operator `POST_K1_K2_K3`. This test does not have physical meaning inevitably, it is primarily a data-processing test.

Modeling a:

- Modeling: 3D, crack with a grid (FEM)
- Resolution of a linear elastic mechanical problem

Modeling b:

- Modeling: 3D, crack not-with a grid (X-FEM)
- Resolution of a linear elastic mechanical problem

Modeling C:

- Modeling: `C_PLAN`, crack with a grid (FEM)
- Resolution of a problem of modal analysis

Modeling D :

- Modeling: `AXIS`, `C_PLAN` and `D_PLAN`, crack with a grid (FEM)
- Resolution of a linear elastic mechanical problem, with variables of order

Modeling E :

- Modeling: `D_PLAN`, crack not-with a grid (X-FEM)
- Resolution of a linear elastic mechanical problem, with variables of order

Although this test is of data-processing nature and that one can be satisfied with a voluntarily brief documentation, certain modelings are more detailed:

- modelings A and B are documented in a complete way;
- modeling C, resulting from CAS-test SDLS114A, is not documented;
- Lmodeling D, resulting from CAS-test FORMA05A has, is not documented;
- LE modeling E, resulting from CAS-test FORMA06A, is not documented.

1 Problem of reference for modelings A and B

1.1 Geometry

The studied structure is a cube of edge 1 measures comprising a plane crack, being at middle height (see [Figure 1.1-a]). If with the problem is dealt by a classical method (modeling A), the crack is with a grid. On the other hand, if method X-FEM is employed (modeling B), the crack is not with a grid, and the geometry is in fact a healthy cube without crack. The crack will then be introduced by functions of levels (level sets) directly into the file orders using the operator `DEFI_FISS_XFEM` [U4.82.08].

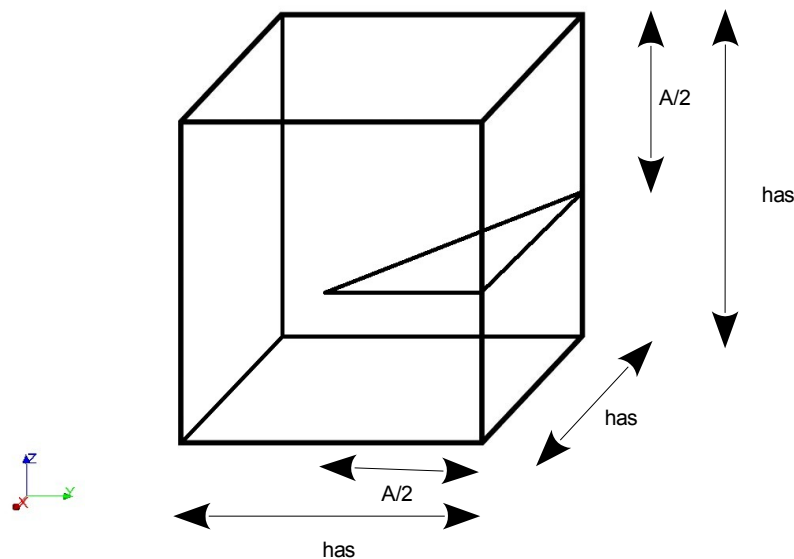


Figure 1.1-a: Geometry of the fissured cube

1.2 Properties materials

The behavior of the structure is elastic and its properties materials are:

Young modulus: $E = 205000 \text{ Mpa}$

Poisson's ratio: $\nu = 0$

1.3 Boundary conditions and loadings

The displacement of the lower face of the structure are blocked whereas a pressure of 1 MPa is applied to the higher face in order to simulate a loading of traction. This makes it possible to request the crack in mode of opening I pure.

2 Modeling a: fissures with a grid

In this modeling, the crack is with a grid, and one uses the standard method of the finite elements to carry out calculation.

2.1 Characteristics of the grid

The structure is modelled by a fissured grid composed of 13874 tetrahedrons (see [Figure 2.1-a]).

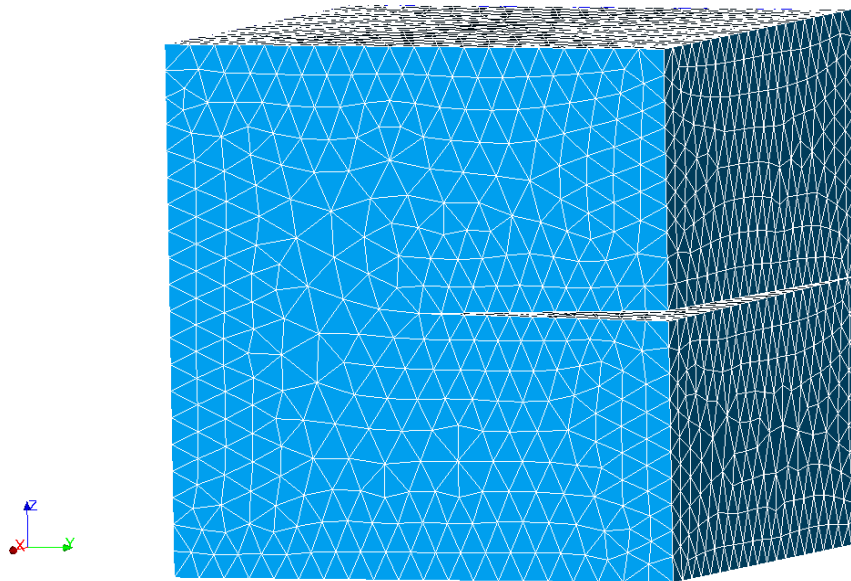


Figure 2.1-a: Fissured grid

2.2 Sizes tested and results

One tests the values of KI on the first three nodes of the bottom of crack. Indeed, the orientation of the crack implies that KI could not be calculated on certain nodes. We test the nodes concerned to check that Code_Aster allots the value of the close node nearest to them or the calculation of KI with been able to be carried out.

Identification	Type of reference	Value of reference
Node 1	'NON_REGRESSION'	212813.877395
Node 2	'NON_REGRESSION'	212813.877395
Node 3	'NON_REGRESSION'	212813.877395

3 Modeling b: fissures X-FEM

In this modeling, the crack is not with a grid any more, but it is represented by level sets:
 $LSN = z - 1/2$ and $LST = -y - x/2 + 1$.

3.1 Characteristics of the grid

The structure is modelled by a grid made up of 15872 tetrahedrons (see [Figure 2.1-a]).

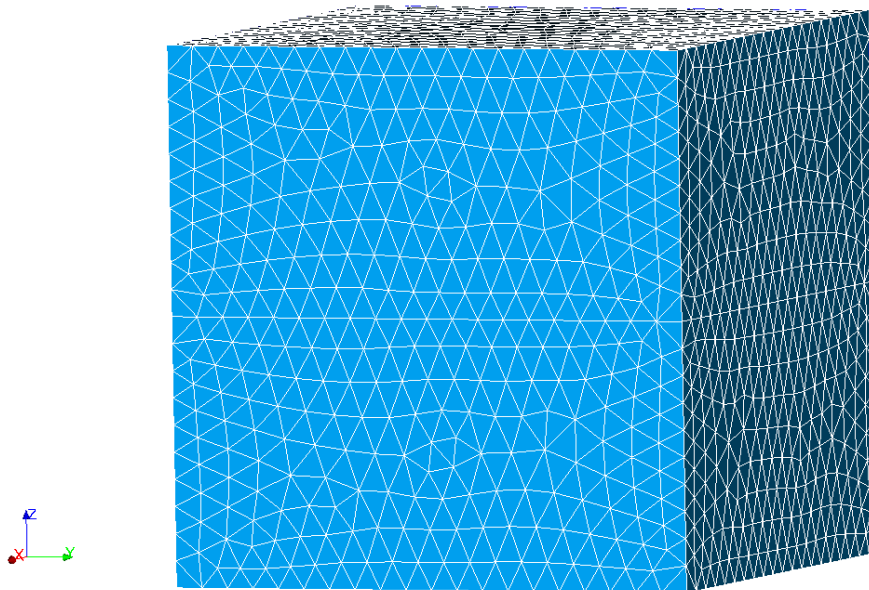


Figure 2.1-a: Healthy grid

3.2 Sizes tested and results

One tests the values of KI on the second point and the last three points of the bottom of crack. Indeed, the orientation of the crack implies that KI could not be calculated on certain points. We test the points concerned to check that *Code_Aster* their allots the value of the close node nearest or calculation to KI with been able to be carried out.

Identification	Type of reference	Value of reference
Point 2	'NON_REGRESSION'	1324885.20838
Point 22	'NON_REGRESSION'	851382.586304
Point 23	'NON_REGRESSION'	851382.586304
Point 24	'NON_REGRESSION'	851382.586304