

## SDLS127 - Harmonic answer of a viscoelastic plate sandwich embedded on an edge

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### Summary:

The objective of this test is to validate the calculation of the harmonic answer of a structure comprising at the same time standard elastic materials, and viscoelastic materials whose properties depend on the frequency.

Three modelings are carried out:

- Modeling A : direct calculation on physical basis, by calculating the assembled matrices frequency by frequency; this modeling is used as reference;
- Modeling b: preliminary calculation of the real clean modes, then harmonic calculation on modal basis;
- Modeling C: preliminary calculation of the real clean modes improved ("beta-modes"), then harmonic calculation on modal basis.

## 1 Problem of reference

### 1.1 Geometry

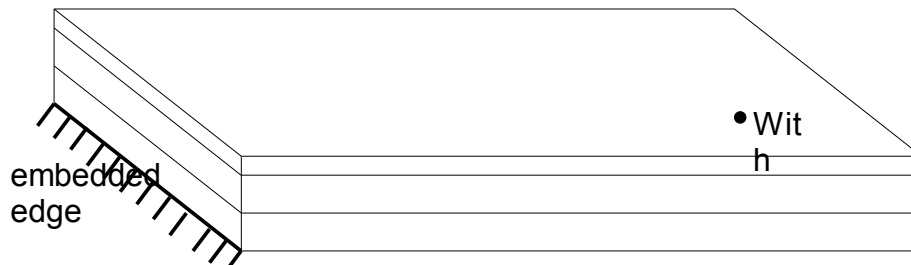


Image 1.1-1: Geometry of the plate sandwich.

Plate rectangular sandwich made up of three layers of different materials:

Side 0.05 m X 0.15 m

Thickness: aluminium (above): 0.5 mm  
viscoelastic material (center): 1 mm  
steel (below): 1 mm

### 1.2 Properties of materials

The material of the layer of the top is aluminium (elastic isotropic); its properties are constant:

- Young modulus  $E = 70\,000\text{ MPa}$
- Poisson's ratio  $\nu = 0,3$
- density  $\rho = 2700\text{ kg/m}^3$
- damping hysteretic  $\eta = 0,001$

The material of the layer of the lower part is steel (elastic isotropic); its properties are constant:

- Young modulus  $E = 210\,000\text{ MPa}$
- Poisson's ratio  $\nu = 0,3$
- density  $\rho = 7800\text{ kg/m}^3$
- damping hysteretic  $\eta = 0,002$

The material of the central layer is viscoelastic (elastomer); some of its properties are dependent on the frequency:

Frequency (Hz)	Real part of the Young modulus $E$ (MPa)	Factor of loss $\eta$
1	23.2	1.1
10	58	0.85
50	145	0.7
100	203	0.6
500	348	0.4
1000	435	0.35
1500	464	0.34

Table 1.2-1 : Properties dependent on the frequency of viscoelastic material.

The others are constant:

- Poisson's ratio  $\nu=0,45$
- density  $\rho=1200 \text{ kg/m}^3$

## 1.3 Boundary conditions and loadings

Boundary conditions:

- embedding on an edge of the layer of steel.

Loading:

- nodal force at point a: FZ=1.

## 1.4 Initial conditions

Without object (harmonic calculation).

## 2 Reference solution

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### 2.1 Method of calculating

The harmonic answer Co-localised to point A is calculated by a direct method, frequency by frequency. Thus, frequency by frequency:

- a viscoelastic material is defined whose properties are interpolated starting from the data of Table 1.2-1 ;
- one calculates the assembled matrices of mass and hysteretic rigidity;
- one résoud the equation of dynamics in physical base (operator `DYNA_LINE_HARM` [U4.53.11]).

### 2.2 Sizes and results of reference

The tests are carried out on frequency response Co-localised to point A to 1 Hz, 100 Hz and 500 Hz.

### 2.3 Uncertainties on the solution

Digital solution.

## 3 Modeling A

### 3.1 Characteristics of modeling

Viscoelastic material: modeling 3D.

Material steel: modeling DKT (the surface elements are the lower skin of the voluminal elements of the viscoelastic layer).

Material aluminium: modeling DKT (the surface elements are the higher skin of the voluminal elements of the viscoelastic layer).

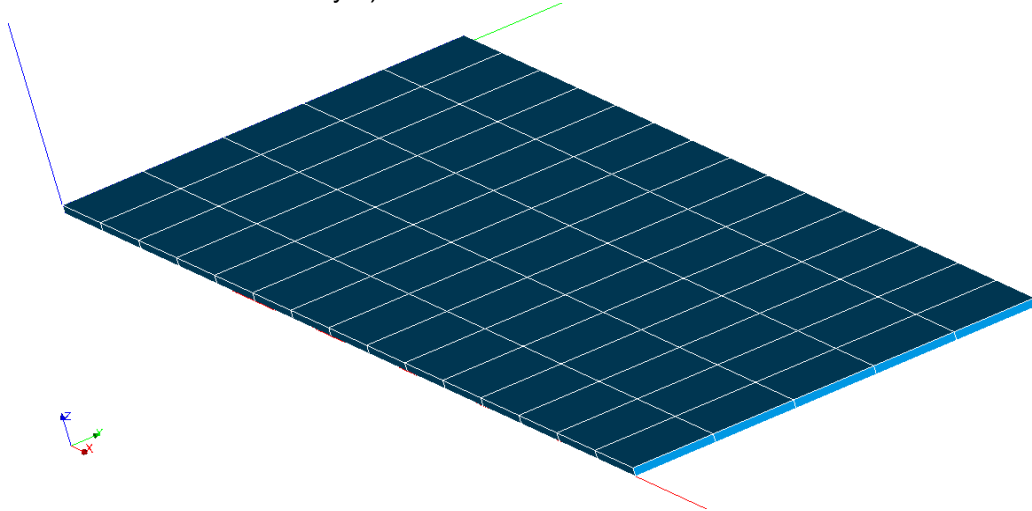


Image 3.1-1 : Grid of the plate sandwich.

### 3.2 Characteristics of the grid

Many nodes 192

Many meshes 349

of which: elements	SEG2	84
	QUAD4	190
	HEXA8	75

### 3.3 Sizes tested and results

This modeling is used as reference, the tests are thus carried out only to check the not-regression of the code.

One tests the values of displacement according to axis Z at point A.

<b>Direct method</b>
<b>Size</b>
DZ (NUME_ORDE=1)
DZ (NUME_ORDE=100)
DZ (NUME_ORDE=500)

## 4 Modeling B

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### 4.1 Characteristics of modeling

Idem that for modeling A.

### 4.2 Characteristics of the grid

Idem that for modeling A.

### 4.3 Sizes tested and results

The method used for calculation of the clean modes is the method "mode real" (TYPE\_MODE='REEL').

One tests the values of displacement according to axis Z at point A.

Method "real mode"	
Size	Reference
DZ (NUME_ORDE=1)	3.84063122275e-04 - 8.77803614739e-05j
DZ (NUME_ORDE=100)	-1.1663671537e-04 - 9.6134604316e-06j
DZ (NUME_ORDE=500)	-1.302768494 e-05 - 1.65977932083 e-06j

## 5 Modeling C

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### 5.1 Characteristics of modeling

Idem that for modeling A.

### 5.2 Characteristics of the grid

Idem that for modeling A.

### 5.3 Sizes tested and results

The method used for calculation of the clean modes is the method “  $\beta$  - mode ” (TYPE\_MODE='BETA').

One tests the values of displacement according to axis Z at point A.

Method “beta mode”	
Size	Reference
DZ (NUME_ORDE=1)	3.84063122275e-04 - 8.77803614739e-05j
DZ (NUME_ORDE=100)	-1.1663671537e-04 - 9.6134604316e-06j
DZ (NUME_ORDE=500)	-1.302768494 e-05 - 1.65977932083 e-06j

**Table 5.3-1: Sizes tested and results of reference for modeling C.**

## 6 Summary of the results

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### Method "real mode"

The got results reveal a maximum error of 2.61% compared to the reference solution.

### Method " $\beta$ -mode "

The got results reveal a maximum error of 2.71% compared to the reference solution.