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## SSLL12 - Lattice of bars under three requests

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### Summary:

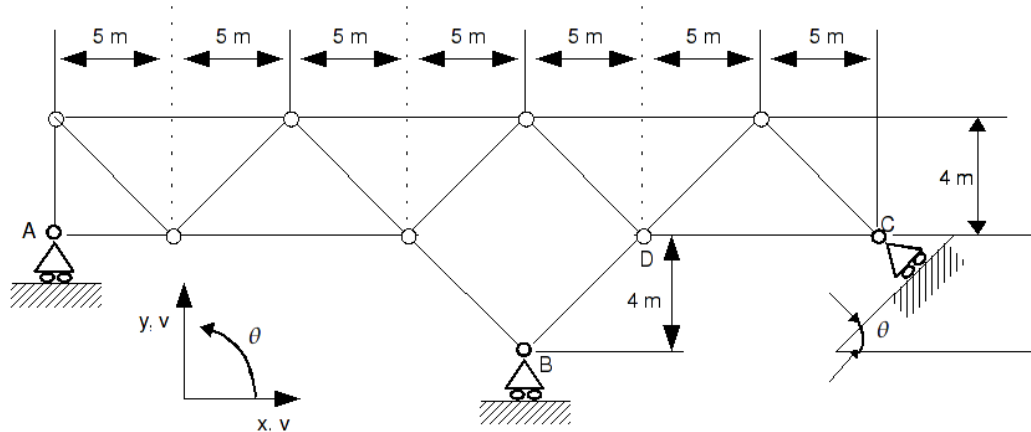
Static answer in linear mechanics of the structures of a triangulated system of pin jointed struts (lattice plan) under 3 requests:

- displacement of support,
- specific forces,
- effect of dilation.

This test makes it possible to validate the element `BAR` under various cases of loading. It validates also the option `LIAISON_OBLIQUE` order `AFFE_CHAR_MECA`.

## 1 Problem of reference

### 1.1 Geometry



### 1.2 Material properties

Isotropic linear elastic material:  $E = 2.1 E + 11 Pa$

Linear dilation coefficient:  $\alpha = 1. E - 05 ^\circ C^{-1}$

### 1.3 Boundary conditions and loadings

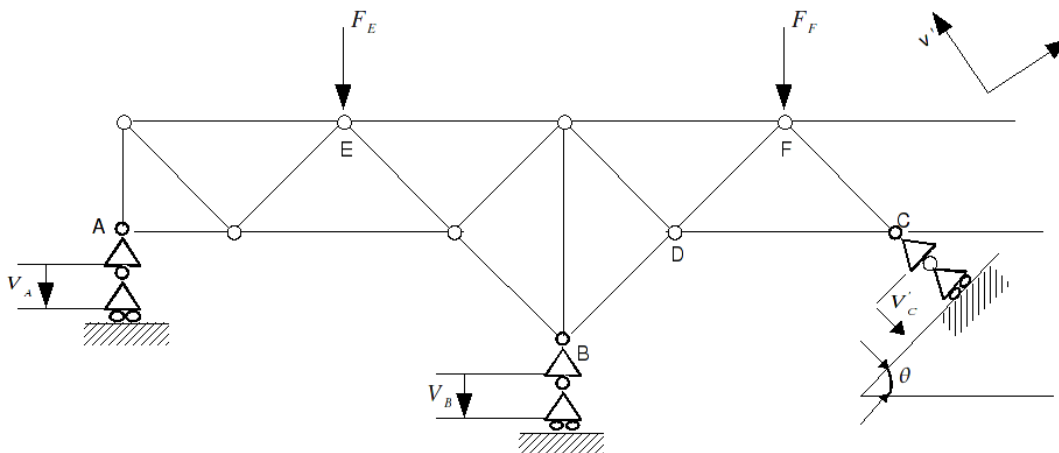
Articulation in  $A$  ( $u_A = v_A = 0$ ).

Support with roller in  $B$  and  $C$  ( $v_B = v'_C = 0$ ).

### 1.4 Initial conditions

Office plurality of 3 requests:

- displacement of support:  $v_A = -0.02 m$ ,  $v_B = -0.03 m$ ,  $v'_C = -0.015 m$
- specific forces:  $F_E = -150 kN$ ,  $F_F = -100 kN$
- effect of dilation of all the bars for a variation in temperature of  $30^\circ C$  compared to the temperature of assembly (geometry of reference).



## 2 Reference solution

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### 2.1 Method of calculating used for the reference solution

Determination of the unknown the hyperstatic one by the method of cut to know the tractive effort.

### 2.2 Results of reference

Not	Size and unit	Value
<i>BD</i>	Tractive effort ( <i>N</i> )	– 8.2112 E+03

### 2.3 Uncertainty on the solution

Analytical solution.

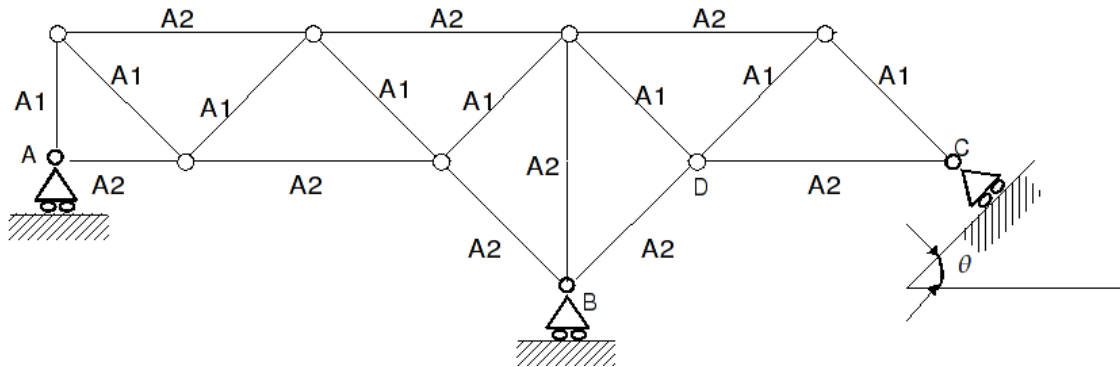
### 2.4 Bibliographical references

[1] Mr. LAREDO, Resistance of materials, Paris, Dunod, 1970, p. 579.

## 3 Modeling A

### 3.1 Characteristics of modeling

Type of modeling used: element BAR.



### 3.2 Characteristics of the grid

$$\theta = 30^\circ, A1 = 1.41 E - 03 \text{ m}^2, A2 = 2.82 E - 03 \text{ m}^2.$$

### 3.3 Sizes tested and results

Identification	Reference	Aster	% difference
Load: thermal dilation			
Option: 'EFGE_ELNO'			
Mesh M10, Node: B, Cmp: N	12946.	1.29541 E+04	0,063
Mesh M16, Node: C, Cmp: N	4285.2	4.28926 E+03	0,095
Mesh M17, Node: C, Cmp: N	- 10189.	- 1.02076 E+04	0,183
Load: specific forces			
Option: 'DEPL'			
Node: E, Cmp: DY	- 1.0566 E-02	- 1.05800 E-02	0,133
Option: 'EFGE_ELNO'			
Mesh M10, Node: B, Cmp: N	- 87137.	- 8.71128 E+04	- 0,028
Mesh M16, Node: C, Cmp: N	24158.	2.41596 E+04	0,007
Mesh M17, Node: C, Cmp: N	- 57524.	- 5.74954 E+04	- 0,050
Load: imposed displacements			
Option: 'EFGE_ELNO'			
Mesh M10, Node: B, Cmp: N	65979.1	6.59757 E+04	- 0,005
Mesh M16, Node: C, Cmp: N	21839.1	2.18453 E+04	0,029
Mesh M17, Node: C, Cmp: N	- 51925.6	- 5.19877 E+04	0,120
Load: office plurality of the 3 requests			
Option: 'EFGE_ELNO'			
Mesh M10, Node: B, Cmp: N	- 8211.2	- 8.18302 E+03	- 0,343
Mesh M16, Node: C, Cmp: N	50282	5.02942 E+04	0,024
Mesh M17, Node: C, Cmp: N	- 1.1964 E+05	- 1.19691 E+05	0,043

### 3.4 Remarks

No deformation of inflection intervenes in the calculation of the solution.

## 4 Summary of the results

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The variations compared to the references are lower than 0.18% for the requests (thermal dilation, specific face, imposed displacement) separate and lower than 0.34% when these requests are cumulated.