
SSLL101 - Piping: Problem of HOVGAARD

Summary:

It is about a linear elastic test, in statics, of a noncoplanar three-dimensional piping comprising elbows. There exists a test in dynamics of same structure (SDLX02) [V2.05.002].

The elements are tested `POU_D_T`, `PIPE (SEG3 and SEG4)` and `TUYAU_6M (SEG3)` via 5 modelings:

- modeling a: 92 elements `POU_D_T` (40 for an elbow), calculation with `MECA_STATIQUE`,
- modeling C: 28 elements `PIPE (SEG3)` (5 for an elbow), calculation with `MECA_STATIQUE`,
- modeling D: 28 elements `TUYAU_6M (SEG3)` (5 for an elbow), calculation with `MECA_STATIQUE`,
- modeling E: 28 elements `PIPE (SEG4)` (5 for an elbow), calculation with `MECA_STATIQUE`,

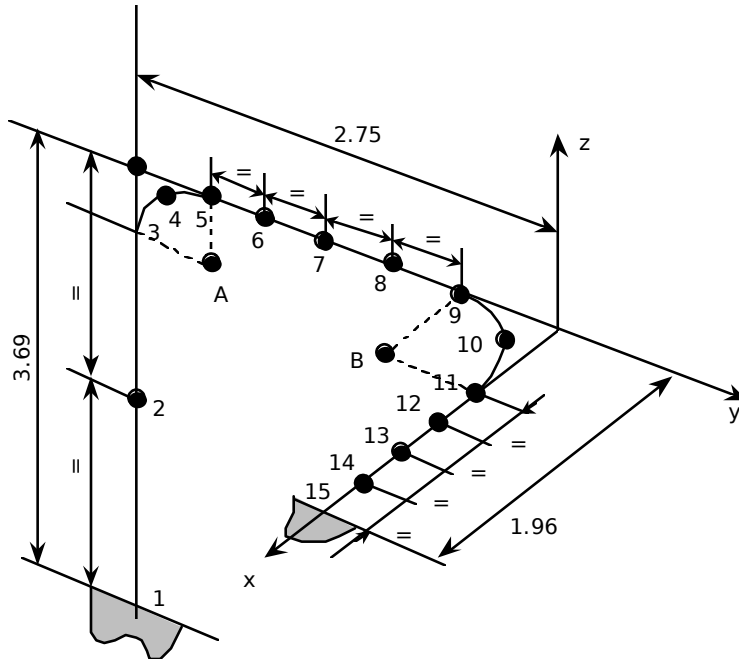
The loadings are of type:

- gravity,
- thermics,
- nodal forces.

1 Problem of reference

1.1 Geometry

Geometry, as well as the points of modeling are represented on the following figure:



$$A \begin{vmatrix} 0. \\ -1.828 \\ -0.922 \end{vmatrix}$$

$$B \begin{vmatrix} 0.922 \\ -0.922 \\ 0. \end{vmatrix}$$

- diameter external of the pipe: 0.185 m
- thickness of the pipe: 6.12 mm
- radius of curvature of the elbows: 0.922 m
- piping full of water

1.2 Material properties

$$E = 1.658 E + 11 Pa$$

$$\nu = 0.3$$

$$\rho = 13404.10 kg/m^3$$

$$\alpha = 0.1288 E - 4/C^\circ$$

1.3 Boundary conditions and loadings

- Items 1 and 15 embedded,
- Loading:
 1. Gravity according to $-z$,
 2. Uniform rise in temperature of $472.22 C^\circ$,
 3. Nodal forces.

Nodes	2	3	4 - 10	5 - 9	6 - 7 - 8	11	01/12/13	14
$F_z (N)$	-	-	-	-	-	-	-117,720	-176,580
	624,897	788,724	327,654	214,839	102,5145	222,687		

2 Reference solution

2.1 Method of calculating used for the reference solution

Reference solutions adopted to check modelings *Code_Aster* are the following ones:

- for modelings *BEAM* : comparison with the codes: *POUX* , *ADL* and *TITUS-T* [bib1], using a modeling of type beam,
- for modelings *PIPE* : comparison with the code *ABAQUS* , using a modeling of type pipe. The number of mode of Fourier (M) used during the calculation of the reference is identical to that used during calculations with *Code_Aster*.

2.2 Results of reference

Cas de Chargement	Displacement as in point 3	Modeling Beam (<i>POUX</i> , <i>ADL</i> , <i>TITUS</i>)	Modeling Pipe: $M=3$ (<i>ABAQUS</i>)	Modeling Pipe: $M=6$ (<i>ABAQUS</i>)
Actual weight	DX	- 0.1658E-3	- 0.16517E-3	- 0.16512E-3
	DY	- 0.2040E-4	- 0.13870E-4	- 0.13946E-4
	DZ	- 0.8010E-5	- 0.80376E-5	- 0.80369E-5
Nodal force	DX	- 0.1651E-3	- 0.16445E-3	- 0.16441E-3
	DY	- 0.2080E-4	- 0.14245E-4	- 0.14320E-4
	DZ	- 0.9516E-5	- 0.10047E-4	- 0.10047E-4
Dilation	DX	- 6.1418E-3	- 6.3277E-3	- 6.3236E-3
	DY	- 13.090E-3	- 13.092E-3	- 13.093E-3
	DZ	16.799E-3	16.798E-3	16.798E-3

2.3 Uncertainty on the solution

Uncertainty on the reference solution is fixed at 2% .

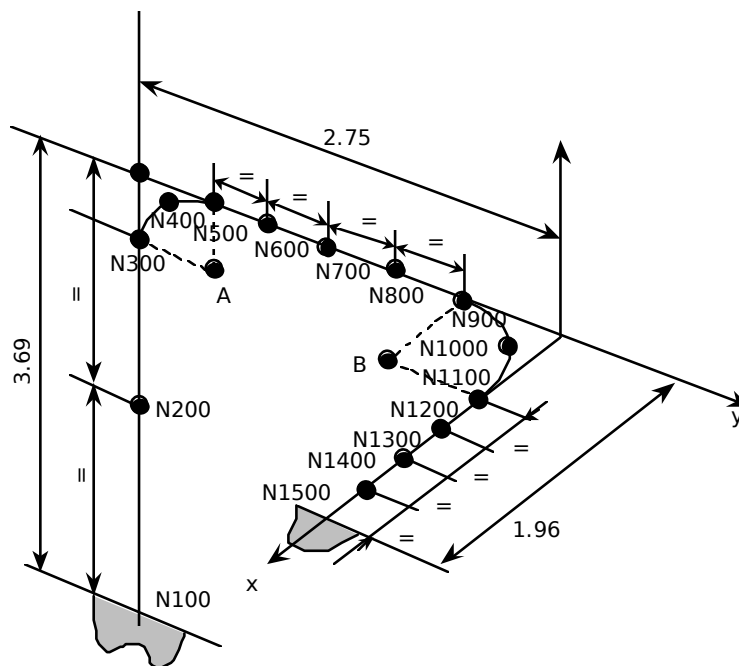
2.4 Bibliographical references

1. M.W. KELLOG Co. Design of Piping Systems. New York, 1956 - Problem n°5.9

3 Modeling A

3.1 Characteristics of modeling

The curved elements are modelled by right elements.
A half curved element is modelled by 20 right elements.



Lengths in meters

3.2 Characteristics of the grid

Many nodes: 93
Number of meshes and type: 92 POU_D_T

3.3 Sizes tested and results

Identification	Displacement	Reference beam	%
	N300 DX	- 0.1658E-3	0.0
Actual weight	DY	- 0.2040E-4	0.02
	DZ	- 0.8010E-5	0.0
	N300 DX	- 0.1651E-3	0.04
Nodal force	DY	- 0.2080E-4	- 0.01
	DZ	- 0.9516E-5	0,004
	N300 DX	- 6.1418E-3	0,007
Dilation	DY	- 13.090E-3	0,012
	DZ	16.799E-3	0,003

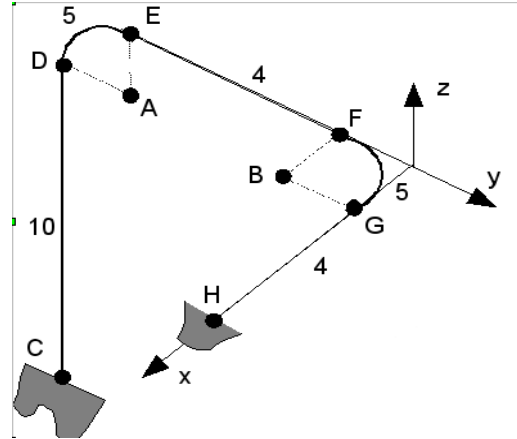
3.4 Notice

Differences between the results *Aster* and the reference solution beam are all lower than 0.04%

4 Modeling C

4.1 Characteristics of modeling

Modeling PIPE (SEG3)



Lengths in meters

Boundary conditions: points *C* and *H*

- DDL beam: $DX = DY = DZ = DRX = DRY = DRZ = 0$
- DDL hull:
 - $UIm = VIm = WIm = 0 (m=2,3)$
 - $UOm = VOm = WOm = 0 (m=2,3)$
 - $WI1 = WO1 = WO = 0$

4.2 Characteristics of the grid

Many nodes: 57
Number of meshes and type: 28 SEG3

4.3 Values tested

Identification	Displacement	Reference pipe ($M = 3$)	%
	Not <i>D</i> <i>DX</i>	- 0.16517E-3	- 0.93
Actual weight	<i>DY</i>	- 0.13870E-4	- 9.80
	<i>DZ</i>	- 0.80376E-5	- 0.24
	Not <i>D</i> <i>DX</i>	- 0.16445E-3	- 0.94
Nodal force	<i>DY</i>	- 0.14245E-4	- 9.61
	<i>DZ</i>	- 0.10047E-4	- 0.20
	Not <i>D</i> <i>DX</i>	- 6.3277E-3	1.99
Dilation	<i>DY</i>	- 13.092E-3	0.08
	<i>DZ</i>	16.798E-3	- 0.93

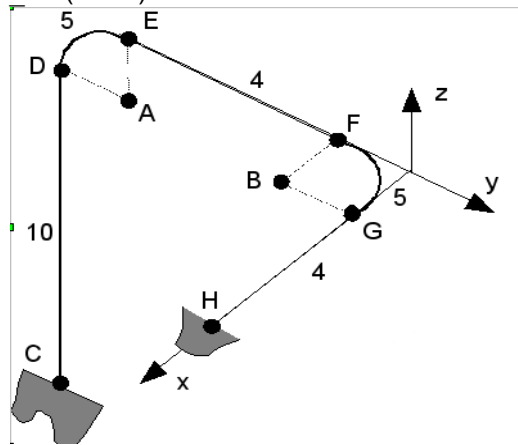
4.4 Notice

Results got with Code_Aster are similar to those of ABAQUS by elements pipes except for displacement *DY* (actual weight and nodal force) where the variation is about 10%.

5 Modeling D

5.1 Characteristics of modeling

Modeling TUYAU_6M (SEG3)



Lengths in meters

Boundary conditions: points *C* and *H*

- DDL beam: $DX = DY = DZ = DRX = DRY = DRZ = 0$
- DDL hull:
 - $UIm = VIm = WIm = 0 (m = 2, 6)$
 - $UOm = VOm = WOm = 0 (m = 2, 6)$
 - $WI1 = WO1 = WO = 0$

5.2 Characteristics of the grid

Many nodes: 57
Number of meshes and type: 28 SEG3

5.3 Sizes tested and results

Identification	Displacement	Reference pipe ($M = 6$)	%
Not <i>D</i>	<i>DX</i>	- 0.16512E-3	- 0.93
Actual weight	<i>DY</i>	- 0.13946E-4	- 9.78
	<i>DZ</i>	- 0.80369E-5	- 0.24
Not <i>D</i>	<i>DX</i>	- 0.16441E-3	- 0.94
Nodal force	<i>DY</i>	- 0.14320E-4	- 9.58
	<i>DZ</i>	- 0.10047E-4	- 0.21
Not <i>D</i>	<i>DX</i>	- 6.3236E-3	1.99
Dilation	<i>DY</i>	- 13.093E-3	0.08
	<i>DZ</i>	16.798E-3	0.49

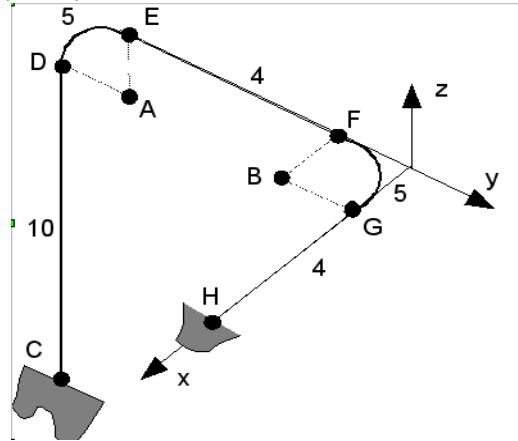
5.4 Notice

Results got with *Code_Aster* are similar to those of ABAQUS for elements pipes except for displacement *DY* (actual weight and nodal force) where the variation is about 10%.

6 Modeling E

6.1 Characteristics of modeling

Modeling PIPE (SEG4)



Lengths in meters

Boundary conditions: points *C* and *H*

- DDL beam: $DX = DY = DZ = DRX = DRY = DRZ = 0$
- DDL hull:
 - $UIm = VIm = WIm = 0 (m=2,3)$
 - $UOm = VOm = WOm = 0 (m=2,3)$
 - $WI1 = WO1 = WO = 0$

6.2 Characteristics of the grid

Many nodes: 85
Number of meshes and type: 28 SEG4

6.3 Sizes tested and results

Identification	Displacement	Reference pipe ($M=3$)	%
Actual weight	Not <i>D</i> <i>DX</i>	-0.16517E-03	-0.22
	<i>DY</i>	-0.13870E-04	-4.73
	<i>DZ</i>	-0.80376E-05	-0.18
Nodal force	Not <i>D</i> <i>DX</i>	-0.16445E-03	-0.37
	<i>DY</i>	-0.14245E-04	-1.74
	<i>DZ</i>	-0.10047E-04	-0.50
Dilation	Not <i>D</i> <i>DX</i>	-6.3277E-03	0.02
	<i>DY</i>	-13.092E-03	0.10
	<i>DZ</i>	16.798E-03	0.27

6.4 Remarks

Grid in SEG4 is obtained starting from a grid SEG3 with the order CREA_MAILLAGE, MODI_MAILLE with the option 'SEG3_4'. It is important that the node medium of SEG3 that is to say well in the medium, it Code_Aster check this condition with a tolerance.

Results got with Code_Aster are similar to those of ABAQUS with elements pipes except for displacement *DY* (actual weight and nodal force) or the variation is about 5% and 2%.

7 Summary of the results

Modeling beam:

The results are similar to the reference solution (modeling beam: average of results of 3 codes).

Modeling pipe:

Results *Code_Aster* are similar to those of ABAQUS (for elements pipes), except for displacement *DY* and for the loadings actual weight and nodal forces where the variation with the reference solution is more important with the meshes SEG3 (10%) that with the meshes SEG4 (5%).

The thermal loading of dilation gives similar results.

This CAS-test makes it possible to test a noncoplanar piping.