

## FORMA06 - Practical works of the formation “advanced Use”: plate multi-fissured in traction

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### Summary:

This test 2D plane deformation, into quasi-static, enters within the framework of the validation of postprocessings in linear elastic breaking process. The plate multi-is fissured. The cracks are represented by method X-FEM.

## 1. Problem of reference

One studies the behavior of a plate multi-fissured in traction. In order not to net the cracks, method X-FEM is used.

One considers an infinite plate in traction, comprising 2 cracks length  $2a$  (see Figure 1-1).

A Pair of Eccentric Parallel Cracks (Isida [1973])

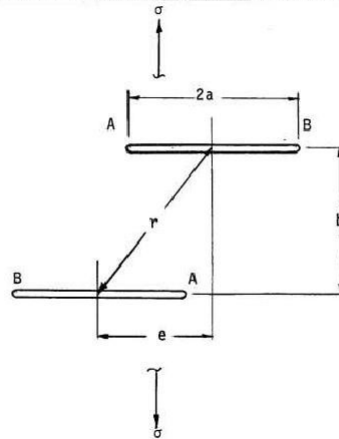


Figure 1-1: geometry of the problem

One proposes to check the abacuses provided by the "Handbook of stress-intensity factors" of G. Sih. The factor of intensity of the constraints  $K_I$  at the point  $A$  is given by the following formula:

$$K_I^A = F\left(\frac{2a}{r}, \frac{e}{b}\right) \sigma \sqrt{\pi a} \text{ where } F\left(\frac{2a}{r}, \frac{e}{b}\right) \text{ is given by the graphics of Figure 2.1.3-1.}$$

## 2. Modeling A

### 2.1. Unfolding of the TP

#### 2.1.1 Geometry and grid with Salomé-Meca

Under Salomé-Méca, carry out the geometry.

One will be able to consider a plate centered in the beginning, of finished size:  $2m$  of with dimensions.

Carry out the grid. It is pointed out that the cracks are not with a grid, one will be able to thus use a regulated grid of quadrangles sufficiently fine everywhere (algorithm 1D = Wire discretization + algorithm 2D = Quadrangle).

#### 2.1.2 Creation of the command file without postprocessing of the rupture

##### a) Reading of the healthy grid and definition of the model not enriched

Reading of the grid refined (LIRE_MAILLAGE) with format MED;
Definition of the finite elements used (AFFE_MODELE, MODELISATION='D_PLAN');
Reorientation of the normals to the elements: one will use MODI_MAILLAGE/ORIE_PEAU_2 D in the same way to direct all the elements, with a turned normal towards outside for the faces to which one

applies the loading;

## b) Definition of the crack and elements X-FEM

Definition of only one fissures horizontal length  $2a=0,3\text{ m}$  (DEFI\_FISS\_XFEM): Utilisez the catalogue of cracks preferably ( FORM\_FISS= ' SEGMENT' )

Modification of the model to take into account elements X-FEM (MODI\_MODELE\_XFEM),

## c) Definition of material, the conditions and resolution of the mechanical problem

Definition and assignment of material (DEFI\_MATERIAU and AFFE\_MATERIAU);

Definition of the limiting conditions and loadings (AFFE\_CHAR\_MECA) on the enriched model :

- Blocking of the rigid modes (DDL\_IMPO on S GROUP\_NO 'N\_A', 'N\_B');
- Application of traction (1 MPa) on 'M\_haut' and 'M\_bas' (PRES\_REP)

Resolution of the elastic problem (MECA\_STATIQUE) on the enriched model.

## d) Postprocessing of displacements and the constraints with X-FEM and visualization with Paravis

Creation of a grid of visualization (POST\_MAIL\_XFEM);

Creation of a model for visualization (AFFE\_MODELE) on the grid created for visualization;

Creation of a field of results on the grid of visualization X-FEM (POST\_CHAM\_XFEM);

Impression of the results to format MED (IMPR\_RESU).

Supplement the command file realized by taking of account 2 cracks, in the case of figure according to:

$$a=0,15 \text{ and } b=0,4 \text{ (either } 2a/b=0,75 \text{ )}$$
$$e=0$$

One is reminded that each call DEFI\_FISS\_XFEM product a crack. For 2 cracks, this order should be called twice .

## 2.1.3 Addition of the postprocessing of the rupture to the command file

### a) Calculation of K with CALC\_G

To calculate the factor of intensity of the constraints (K1) (OPTION=' CALC\_K\_G' ) .

To use the result of MECA\_STATIQUE (RESULT) .

To supplement information at once THETA :

- bottom of crack, by specifying the number of the bottom (in your case there are 2 funds of crack A and B)
- rays of the crown of the field theta ( R\_INF , R\_SUP ), to define according to the grid used.

The order CALC\_G producing a structure of data of the type counts, one needs l mprimer results in a table with IMPR\_TABLE .

### b) Calculation of K with POST\_K1\_K2\_K3

To calculate K with POST\_K1\_K2\_K3 :

- to use the result of MECA\_STATIQUE (RESULT)

- to inform the bottom of crack
- to inform the parameter `ABSC_CURV_MAXI`
- to print the results in a table ( `IMPR_TABLE` )

Note: not to take account of alarm in `CALC_CHAMP` which specifies that `EXCIT` should be added.

Compare got results with the solution of Handbook.

To go further, one will be able:

- to prolong the abacuses for  $2a/r > 0.9$  (for example  $2a/r = 1$  ),
- to study the smoothness of the grid,
- to make a parametric study for  $e = [0 ; 2b]$  (to think of using python),
- to study other configurations (inclined cracks, addition of other cracks...).

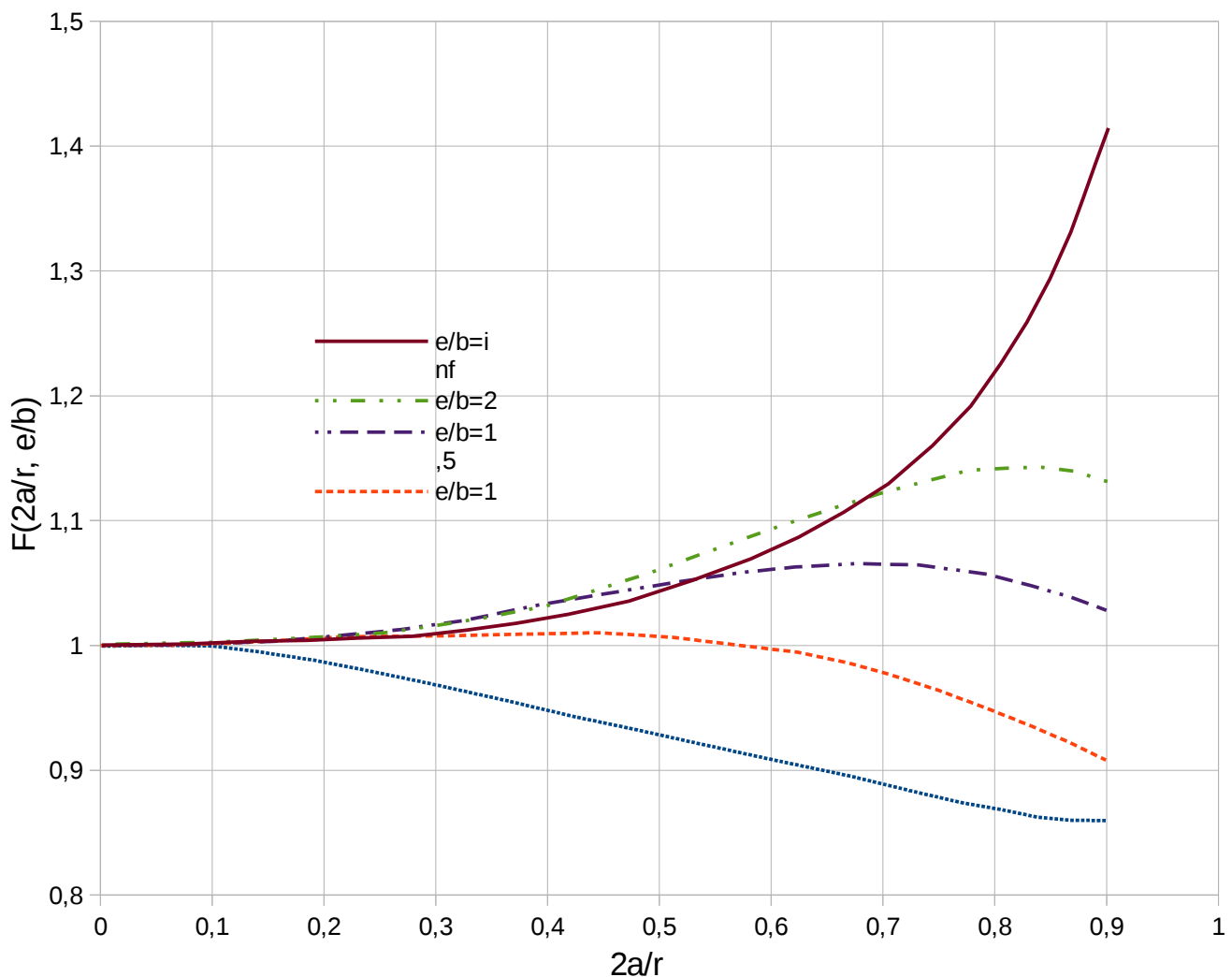


Figure 2.1.3-1: Abacus