

## SSLS104 - Cylindrical hull pinch with diaphragm

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### Summary:

One treats in linear elasticity the case of a cylinder formed by two circular funds at the two ends and gripped with mid-length.

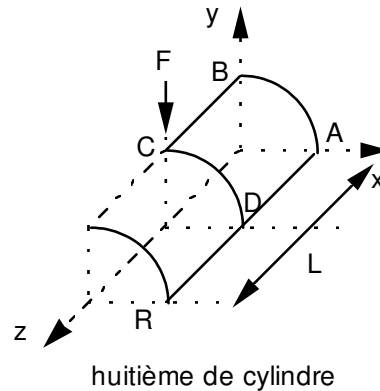
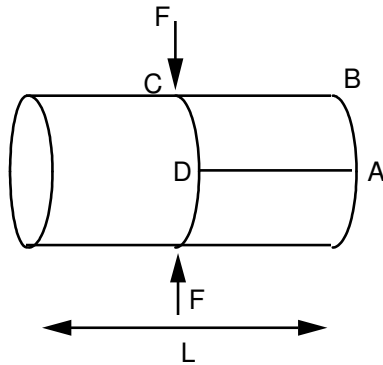
This makes it possible to treat the modes of deformation inextensionnels and a membrane behavior complexes due to the diaphragms.

The value tested is the arrow at the point of application of the force.

Three modelings: DKT, COQUE\_3D QUAD9 and COQUE\_3D TRIA7.

## 1 Problem of reference

### 1.1 Geometry



Longueur  $L = 600$   
Rayon  $R = 300$   
Epaisseur  $t = 3$

Coordinates of the points:

	$A$	$B$	$C$	$D$
$x$	300.	0.	0.	300.
$y$	0.	300.	300.	0.
$z$	0.	0.	300.	300.

### 1.2 Material properties

$E = 3 \cdot 10^6 \text{ Pa}$   
 $\nu = 0.3$   
 $A_{CIS} = 0.8333$

### 1.3 Boundary conditions and loadings

Rigid diaphragm at each end:

$$u = v = 0, \quad \theta_z = 0$$

Specific force in  $C$  :

$$F = 1. N$$

## 2 Reference solution

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### 2.1 Method of calculating used for the reference solution

The parameters of with the dealt problem and the results of reference are explicitly given in the publication quoted below.

### 2.2 Results of reference

Displacement of the point  $C$  according to  $y$ .

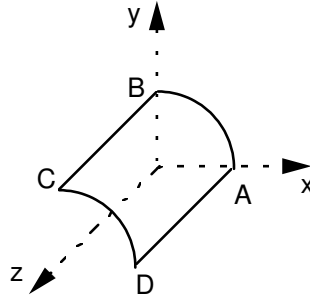
### 2.3 Bibliographical references

- Thomas J.R HUGHES, Ted BELYTSCHKO. Race notes for Recent advances in nonlinear finite element analysis. Volume III - p 238 and 239 (1990).

## 3 Modeling A

### 3.1 Characteristics of modeling

Element of hull DKT



Modeling of a eighth of plate

Cutting:

10 on  $AD$  and  $BC$   
16 on  $AB$  and  $DC$  : 364 meshes TRIA3

Limiting conditions:

in all the nodes of:

arc ( $AB$ )

arc ( $CD$ )

segment)  $BC$  (

segment)  $AD$  (

in  $C$

in  $D$

DDL\_IMPO:

(GROUP\_NO: AB DX: 0. , DY: 0. , DRZ: 0. )

(GROUP\_NO: CD DZ: 0. , DRX: 0. , DRY MARTINI: 0. )

(GROUP\_NO: BCsansBC DX: 0. , DRY MARTINI: 0. , DRZ: 0. )

(GROUP\_NO: ADsansAD DY: 0. , DRX: 0. , DRZ: 0. )

(GROUP\_NO: C DX: 0. , DRZ: 0. )

(GROUP\_NO: D DY: 0. , DRZ: 0. )

Loading:

with the node  $C$  : (GROUP\_NO: C FY: -0.25 )

Names of the nodes:

Not  $A$   $N04$

Not  $B$   $N02$

Not  $C$   $N01$

Not  $D$   $N03$

### 3.2 Characteristics of the grid

Many nodes: 209

Many meshes and types: 364 TRIA3

### 3.3 Values tested

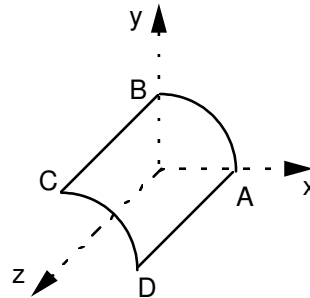
Identification	Reference
Not $C$ displacement $v$	$-1.8248 \cdot 10^{-5}$

With 1,366 nodes:  $-1.8511 F$  in  $C$ .

## 4 Modeling B

### 4.1 Characteristics of modeling

Element of hull 3D MEC3QU9H



Modeling of a eighth of plate

Cutting:

4 on  $AD$  and  $BC$   
8 on  $AB$  and  $DC$  : 32 meshes QUAD9

Limiting conditions:

in all the nodes of:

arc ( $AB$ )	DDL_IMPO: (GROUP_NO: AB DX: 0. , DY: 0. , DRZ: 0. )
arc ( $CD$ )	(GROUP_NO: CD DZ: 0. , DRX: 0. , DRY MARTINI: 0. )
segment) $BC$ (	(GROUP_NO: BCsansBC DX: 0. , DRY MARTINI: 0. , DRZ: 0. )
segment) $AD$ (	(GROUP_NO: ADsansAD DY: 0. , DRX: 0. , DRZ: 0. )
in $C$	(GROUP_NO: C DX: 0. , DRZ: 0. )
in $D$	(GROUP_NO: D DY: 0. , DRZ: 0. )

Loading:

with the node  $C$  : (GROUP\_NO: C FY: -0.25 )

Names of the nodes:

Not $A$	$N01$
Not $B$	$N02$
Not $C$	$N03$
Not $D$	$N04$

### 4.2 Characteristics of the grid

Many nodes: 121  
Many meshes and types: 32 QUAD9

### 4.3 Values tested

Identification	Reference
Not $C$ displacement $v$	$-1.8248 \cdot 10^{-5}$

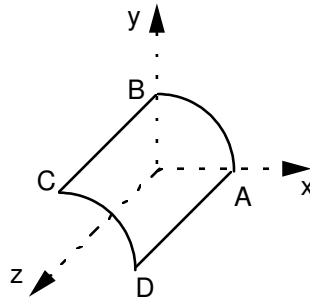
## 4.4 Remarks

For a grid of 60 meshes QUAD9 and 213 nodes (corresponding to cutting 6 on  $AD$  and  $BC$  and 10 on  $AB$  and  $DC$ ), displacement  $v$  at the point  $C$  is worth  $-1.8011 \cdot 10^{-5}$ .

## 5 Modeling C

### 5.1 Characteristics of modeling

Element of hull MEC3TR7H



Modeling of a eighth of plate

Cutting:

10 on  $AD$  and  $BC$

18 on  $AB$  and  $DC$  : 360 meshes TRIA7

Limiting conditions:

in all the nodes of:

arc ( $AB$ )

arc ( $CD$ )

segment)  $BC$  (

segment)  $AD$  (

in  $C$

in  $D$

DDL\_IMPO:

(GROUP\_NO: AB DX: 0. , DY: 0. , DRZ: 0. )

(GROUP\_NO: CD DZ: 0. , DRX: 0. , DRY MARTINI: 0. )

(GROUP\_NO: BCsansBC DX: 0. , DRY MARTINI: 0. , DRZ: 0. )

(GROUP\_NO: ADsansAD DY: 0. , DRX: 0. , DRZ: 0. )

(GROUP\_NO: C DX: 0. , DRZ: 0. )

(GROUP\_NO: D DY: 0. , DRZ: 0. )

Loading:

with the node  $C$  : (GROUP\_NO: C FY: -0.25 )

Names of the nodes:

Not  $A$  N01

Not  $B$  N02

Not  $C$  N03

Not  $D$  N04

### 5.2 Characteristics of the grid

Many nodes: 777

Many meshes and types: 360 TRIA7

### 5.3 Values tested

Identification	Reference
Not $C$ displacement $v$	$-1.8248 \cdot 10^{-5}$



## 5.4 Remarks

For a grid with 500 meshes TRIA7 and 1071 nodes (cutting 10 on  $AD$  and  $BC$ , 25 on  $AB$  and  $DC$ ), a displacement is obtained  $v$  at the point  $C$  of  $-1.7723 \cdot 10^{-5}$ . The relative error on displacement  $v$  in  $C$  is then of 2.88%. The results with this element for light grids is thus not very good and improves relatively little with an increase amongst meshes.

## 6 Summary of the results

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With regard to the elements:

DKT:

The result is better with a finer grid (1366 nodes) which leads to an error < 1.5 %.

MEC3QU9H:

The result is acceptable with relatively few elements (compared with DKT). By increasing appreciably the number of elements (60 instead of 32), the error is < 1.3%.

MEC3TR7H:

Result little satisfying even with a fine grid leading to a great total number of nodes for MEC3TR7H (777 for MEC3TR7H to compare with 209 for DKT and 121 for MEC3QU9H). To arrive at an error lower than 2.9%, that requires one very a large number of nodes (1071). It seems recognized that this element is less good than MEC3QU9H.