

## SSLS133 - Flexbeam with variable thickness

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### Summary:

This test represents a quasi-static calculation of a flexbeam with variable thickness. It is embedded at an end, and is subjected to a vertical force at the other end. This test makes it possible to test the elements of voluminal hull SHB8 and SHB20 to manage the variations thicknesses. Four modelings are tested:

Finite elements SHB8 for a linear variation thickness of the plate (modeling  $A$  ).

Finite elements SHB20 for a linear variation thickness of the plate (modeling  $B$  ).

Finite elements SHB8 for a quadratic variation thickness of the plate (modeling  $C$  ).

Finite elements SHB20 for a quadratic variation thickness of the plate (modeling  $D$  ).

Displacements obtained are compared with the elastic analytical solution of a beam in inflection. This test makes it possible to show the capacities and the limits of the elements SHB8 and SHB20 to manage the variations thicknesses.

## 1 Problem of reference

### 1.1 Geometry

#### 1.1.1 Plate with thickness varying linearly

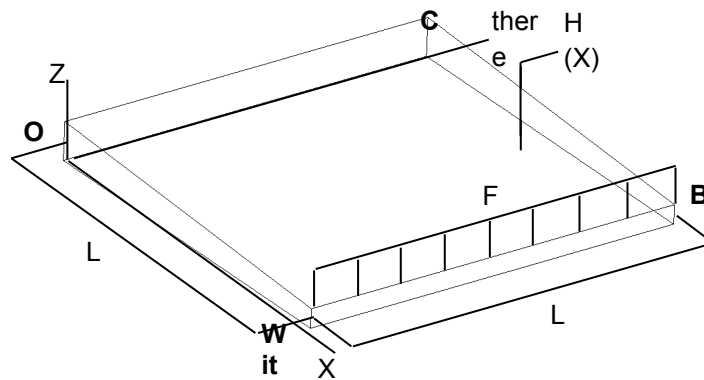


Figure 1.1.1-1 :

Length  $L=100\text{ m}$  , width  $l=100\text{ m}$  .

The thickness  $h$  vary linearly:

$$h(x) = ax + b$$

We pose  $h(x=0)=h_1=10\text{ m}$  and  $h(x=L)=h_2=5\text{ m}$  what gives us:

$$a = (h_2 - h_1)/L \text{ and } b = h_1$$

#### 1.1.2 Plate with thickness varying quadratically

The thickness  $h$  vary in a quadratic way:

$$h(x) = ax^2 + bx + c$$

We pose  $h(x=0)=h_1=10\text{ m}$  ,  $h(x=L)=h_2=5\text{ m}$  and  $h(x=L/2)=h_{12}=6,25\text{ m}$  what gives us

$$a = (2(h_1 + h_2) - 4h_{12})/L^2 , b = (4h_{12} - h_2 - 3h_1)/L \text{ and } c = h_1$$

### 1.2 Material properties

Young modulus:  $E = 2 \cdot 10^{11} \text{ Pa}$

Poisson's ratio:  $\nu = 0.0$

## 1.3 Boundary conditions and loadings

Boundary conditions:

Embedded on the side  $OC$  :  $u=v=w=0$  ,  $\theta_x=\theta_y=\theta_z=0$

Loading:

At the end  $AB$  , one load uniformly distributed of resultant:

Force parallel with the axis  $Z$  ;  $F_z=1N$

## 2 Reference solution

### 2.1 Method of calculating used for the reference solution

The results of reference are got by the theory of the elastic beams.

In the case of a linear variation thickness, vertical displacement at the end  $AB$  is given by [1]:

$$w(x) = -\frac{FL^2}{2EI_{y_1}c^3} \frac{\left(2Lcx + c^2x^2 - c^3x^2 + 2L(L+cx) \ln\left(\frac{L}{L+cx}\right)\right)}{(L+cx)}$$

With

$$c = \left(\frac{I_{y_2}}{I_{y_1}}\right)^{\frac{1}{3}} - 1 \quad \text{and} \quad I_{y_i} = \frac{bh_i^3}{12}$$

In the case of a quadratic variation thickness, it is possible to find a formula exact of displacement. However its general expression is sufficiently complex not to be able to be written here. We formulated the approximate function of vertical displacement according to  $x$  of our case:

$$w(x) = 3 \cdot 10^{-8} \frac{2x-200}{x^2-200x+20000} + 6 \cdot 10^{-10} \arctan(0.01x-1) - 3 \cdot 10^{-12}x + 7.71238 \cdot 10^{-10} m$$

### 2.2 Sizes and results of reference

Displacement of the points  $A$  and  $B$  according to  $Z$ .

### 2.3 Bibliographical references

[1] [V3.01.400] SSSL400 – non-prismatic Beam, subjected to efforts specific or distributed.

## 3 Modeling A

### 3.1 Characteristics of modeling

Element SHB8 and thickness varying linearly

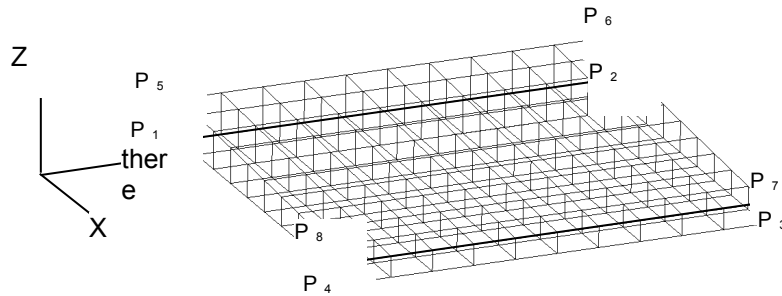


Figure 3.1-1 : Grid of modeling A

Cutting: a regular grid is considered in this modeling.

Regular grid:

100 meshes SHB8 : 10 according to the width, 10 according to the length, 1 according to the thickness

Boundary conditions:

All nodes inside the side  $P_1P_2P_6P_5$  : following blocked displacement  $X$

All nodes on the edge  $P_1P_5$  : following blocked displacement  $Y$

All nodes on the edge  $P_2P_1$  : following blocked displacement  $Z$

Loading:

Force linearly distributed on the edge  $P_8P_7$  :  $F = 1$

Name of the nodes:

Not $P_1$	N022	Not $P_5$	N020
Not $P_2$	N002	Not $P_6$	N001
Not $P_3$	N102	Not $P_7$	N100
Not $P_4$	N172	Not $P_8$	N171

### 3.2 Characteristics of the grid

Many nodes: 242

Many meshes and types: 100 SHB8

### 3.3 Sizes tested and results

Regular grid:

Not	Size in unit	Reference	% difference
P <sub>7</sub>	displacement W ( m )	3.2710 10 <sup>-10</sup>	+0,004
P <sub>8</sub>	displacement W ( m )	3.2710 10 <sup>-10</sup>	+0,004
POINT 1 MESH 1	SIEF_ELGA	0.0543525374822	0.1 %
POINT 2 NETS 1	SIEF_ELGA	0.0322992227094	0,1 %
POINT 3 NETS 1	SIEF_ELGA	0,0	1E-9 %
POINT 4 NETS 1	SIEF_ELGA	-0.0322734188761	0,1 %
POINT 5 NETS 1	SIEF_ELGA	-0.0542794829818	0,1 %
N22 MESH 1	IFGM_ELNO	0.0543350532544	0.1 %
N20 MESH 1	IFGM_ELNO	0.0322992227094	0,1 %

One also tests analytical fields of equivalent constraints of Von Mises.

## 4 Modeling B

### 4.1 Characteristics of modeling

Element SHB20 and thickness varying linearly

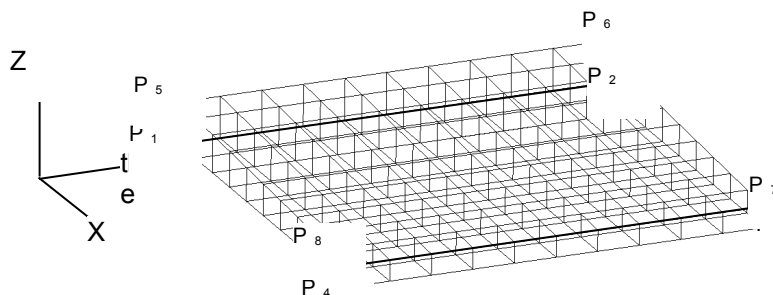


Figure 4.1-1 : Grid of modeling B

Cutting: a regular grid is considered in this modeling.

Regular grid:

100 meshes SHB20 : 10 according to the width, 10 according to the length, 1 according to the thickness

Boundary conditions:

All nodes inside the side  $P_1 P_2 P_6 P_5$  : following blocked displacement  $x$

All nodes on the edge  $P_1 P_5$  : following blocked displacement  $y$

All nodes on the edge  $P_2 P_1$  : following blocked displacement  $z$

Loading:

Force linearly distributed on the edge  $P_8 P_7$  :  $F = 1$

Name of the nodes:

Not P <sub>1</sub>	N347	Not P <sub>5</sub>	N340
Not P <sub>2</sub>	N579	Not P <sub>6</sub>	N572
Not P <sub>3</sub>	N006	Not P <sub>7</sub>	N002
Not P <sub>4</sub>	N074	Not P <sub>8</sub>	N067

## 4.2 Characteristics of the grid

Many nodes: 803

Many meshes and types: 100 SHB20

## 4.3 Sizes tested and results

Regular grid:

Not	Size in unit	Reference	Aster	% difference
P <sub>7</sub>	displacement W ( m )	3.2710 10 <sup>-10</sup>	3.2866 10 <sup>-10</sup>	+0,476
P <sub>8</sub>	displacement W ( m )	3.2710 10 <sup>-10</sup>	3.2866 10 <sup>-10</sup>	+0,476

## 5 Modeling C

### 5.1 Characteristics of modeling

Element SHB8 and thickness varying quadratically

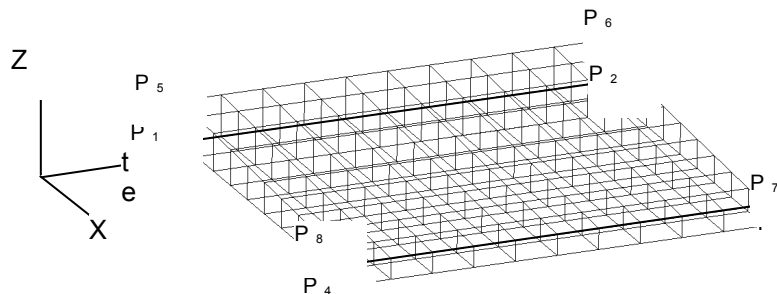


Figure 5.1-1 : Grid of modeling C

The characteristics are the same ones as for modeling A

Name of the nodes:

Not P <sub>1</sub>	N005	Not P <sub>5</sub>	N003
Not P <sub>2</sub>	N006	Not P <sub>6</sub>	N004
Not P <sub>3</sub>	N008	Not P <sub>7</sub>	N002
Not P <sub>4</sub>	N007	Not P <sub>8</sub>	N001

### 5.2 Characteristics of the grid

The grid is the same one as modeling A except for the thickness which varies here in a quadratic way.

## 5.3 Sizes tested and results

Regular grid:

Not	Size in unit	Reference	Aster	% difference
P <sub>7</sub>	displacement W ( m )	4.7124 10 <sup>-10</sup>	5.1212 10 <sup>-10</sup>	9 %
P <sub>8</sub>	displacement W ( m )	4.7124 10 <sup>-10</sup>	5.1212 10 <sup>-10</sup>	9 %



## 6 Modeling D

### 6.1 Characteristics of modeling

Element SHB20 and thickness varying quadratically

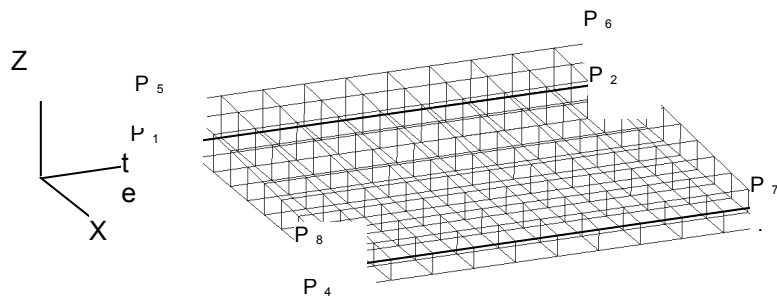


Figure 6.1-1 : Grid of modeling D

The characteristics are the same ones as for modeling *B*

Name of the nodes:

Not P <sub>1</sub>	N005	Not P <sub>5</sub>	N003
Not P <sub>2</sub>	N006	Not P <sub>6</sub>	N004
Not P <sub>3</sub>	N008	Not P <sub>7</sub>	N002
Not P <sub>4</sub>	N007	Not P <sub>8</sub>	N001

### 6.2 Characteristics of the grid

The grid is the same one as modeling *B* except for the thickness which varies here in a quadratic way.

### 6.3 Sizes tested and results

Regular grid:

Not	Size in unit	Reference	Aster	% difference
P <sub>7</sub>	displacement W ( m )	4.7124 10 <sup>-10</sup>	4.6754 10 <sup>-10</sup>	-0,784
P <sub>8</sub>	displacement W ( m )	4.7124 10 <sup>-10</sup>	4.6754 10 <sup>-10</sup>	-0,784

## 7 Summary of the results

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In the case of a variation linare thickness of the plate, good solutions are obtained some is the finite element used (SHB8 or SHB20).

When the geometrical variation is of a quadratic nature, elements SHB20 provide more precise results (error  $< 1\%$  ) that elements SHB8 (error  $< 9\%$  ).