

## TPLS100 - Infinite plate subjected to antisymmetric flows

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### Summary:

The purpose of this test is to test the model of thermal hull linear with three fields (`MODELING`: 'HULL' or 'COQUE\_PLAN') by comparison with an analytical solution, for an infinite plate subjected to a couple of stationary antisymmetric heat flows on its two half-faces, in stationary mode.

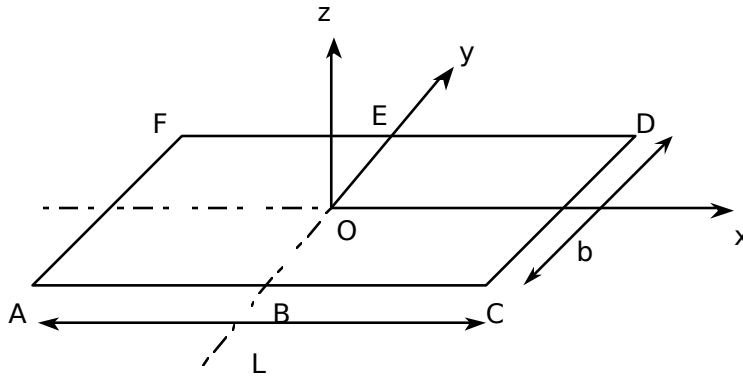
The equation of heat is solved in hover, with a linear, isotropic, homogeneous conduction.

Two modelings: With for the finite elements of surface hull (triangles) and B for the linear elements (segments).

One simultaneously tests in each modeling the elementary orders and the total order `THER_LINEAIRE`.

## 1 Problem of reference

### 1.1 Geometry



Length:  $L = 20\text{mm}$   
Width:  $b = 2\text{mm}$   
Thickness:  $h = 4\text{mm}$

### 1.2 Material properties

Conductivity  $\lambda = 4.5 \text{ W/mm/}^\circ\text{C}$

Voluminal heat:  $\rho C_p = 0. \text{ J/}^\circ\text{C.mm}^3$

### 1.3 Boundary conditions and loadings

Worthless temperature on the average layer of the plate:

$TEMP = 0.$

Flow imposed on the upper surface  $(ABEF)^+$

$flux^+ = 30. \text{ W/mm}^2/^\circ\text{C}$

Flow imposed on the upper surface  $(ABEF)^-$

$flux^- = -30. \text{ W/mm}^2/^\circ\text{C}$

## 2 Reference solution

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### 2.1 Method of calculating used for the reference solution

#### Analytical

For more details to refer to the document [R3.11.01] and the note [bib1].

### 2.2 Results of reference

- Temperature in higher skin,
- Flow into cubes nodes placed on the axis  $Ox$  in higher skin.

### 2.3 Uncertainty on the solution

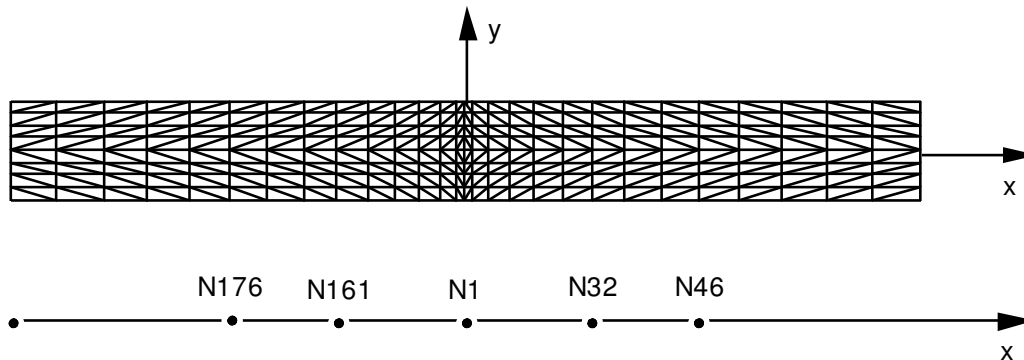
Analytical solution.

### 2.4 Bibliographical references

- S. ANDRIEUX, F. VOLDOIRE HI-71/7131 - Formulation of a model of thermics for the thin hulls (12/7/90).

## 3 Modeling A

### 3.1 Characteristics of modeling



Cutting: 28 elements in length,  
8 elements in width.

Boundary conditions - loading:

```
TEMP_IMPO (ALL = ' oui', TEMP=0.)
FLUX_REP (GROUP_MA =GRSD2, FLUN_INF=-30.
          FLUN_SUP=30.)
```

### 3.2 Characteristics of the grid

Many nodes: 969

Many meshes and types: 448 meshes TRIA6

### 3.3 Sizes tested and results

Identification	Reference
TEMP_SUP :	
node N201 (-10.,0)	13.3321
node N176 (-5.15,0)	13.2565
node N161 (-2.8,0)	12.7462
node N1 (0.,0.)	6.6666
node N32 (28,0.25)	0.5870
node N46 (5.15,0)	0.07679
Flow component X :	
node N176	
mesh M297	0.2992
mesh M289	0.2992
mesh M290	0.2992
median value	0.2992
node N161	
mesh M265	2,287
mesh M266	2,287
mesh M273	2,287
median value	2,287
node N1	
mesh M1	25.98
mesh M225	25.98

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mesh M337	25.98
median value	25.98

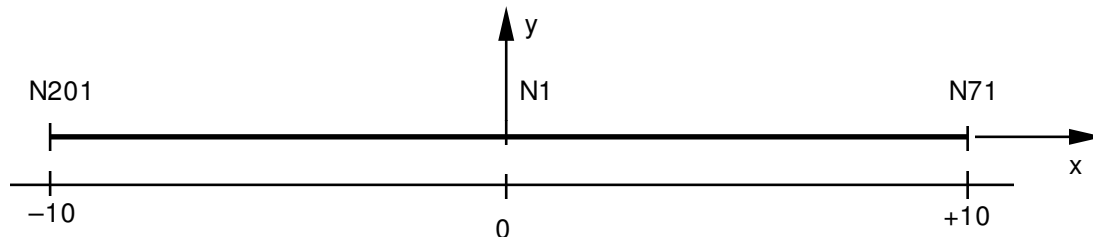
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## Contents of the file results

- Temperatures with the nodes,
- heat flow to the nodes in higher wall,
- values tested deferred above.

## 4 Modeling B

### 4.1 Characteristics of modeling



Cutting: 28 linear elements in length, (even progression of meshes that in the grid of modeling A).

Boundary conditions - loading:

```
TEMP_IMPO (ALL = ' oui', TEMP=0.)  
FLUX_REP (GROUP_MA = GRSD2, FLUX_INF=-30.  
FLUX_SUP=30.)
```

### 4.2 Characteristics of the grid

Many nodes: 57

Many meshes and types: 28 meshes SEG3

### 4.3 Sizes tested and results

Identification	Reference
TEMP_SUP:	
node N201 (-10.,0)	13.3321
node N176 (-5.15,0)	13.2565
node N161 (-2.8,0)	12.7462
node N1 (0.,0.)	6.6666
node N46 (5.15,0)	0.07679

#### Contents of the files results

- Temperatures with the nodes on the upper surface,
- values tested deferred above.

## 5 Summary of the results

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In modeling A with meshes `TRIA6`, one notes that the variations on flows are lower than 1%, except in the zones where those are very weak.