

TTLL01 - Thermal shock on an infinite wall

Summary:

Transitory linear thermics,
elements 2D and 3D (7 modelings),
interests of the test:

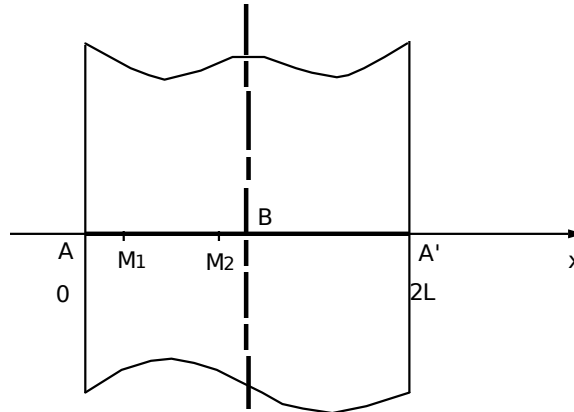
- test the algorithm of linear thermics transitory with change of step of time,
- imposed temperature (with discontinuity),
- filing of some not of time.

The shock is modelled in 2 different ways:

- by a linear slope: $\Delta T = 100.$ in 10^{-3} second,
- by true a discontinuity of imposed temperature.

1 Problem of reference

1.1 Geometry



$$\begin{aligned}\bar{AA}' &= 2L = 2 \text{ m} \\ x(M1) &= 0.2 \text{ m} \\ x(M2) &= 0.8 \text{ m}\end{aligned}$$

1.2 Material properties

$$\begin{aligned}\lambda &= 1 \text{ W/m}^\circ\text{C} \\ \rho C_p &= 1 \text{ J/m}^3\text{ }^\circ\text{C}\end{aligned}$$

1.3 Boundary conditions and loadings

- $A: T(0, t) = T_p = 100^\circ\text{C}$
for $t > 0$
- $A': T(2L, t) = T_p = 100^\circ\text{C}$

1.4 Initial conditions

$$T(x, 0) = 0^\circ\text{C} \quad \text{for all } x$$

1.5 Precise details concerning modelings

Discretization in time (t) :

The thermal shock requires a "fine" discretization in time close to $t = 0$.

The goal of the test being to validate the various elements (various modelings), we chose a single discretization in time:

10	not for	$[0., 1.E-3]$	that is $\Delta t = 10^{-4} \text{ s}$ to say
9	not for	$[1.E-3, 1.E-2]$	that is $\Delta t = 10^{-3} \text{ s}$ to say
9	not for	$[1.E-2, 1.E-1]$	that is $\Delta t = 10^{-2} \text{ s}$ to say
9	not for	$[1.E-1, 1.]$	that is $\Delta t = 10^{-1} \text{ s}$ to say
10	not for	$[1., 2.]$	that is $\Delta t = 10^{-1} \text{ s}$ to say

The shock is defined in two different ways:

- for modeling B, it is about a true shock (T_p is discontinuous):

$$\begin{cases} T_p^-(A) = 0. \\ T_p^+(A) = 100. \end{cases}$$

- for modelings A, C, D, E, F, G , it is about a linear slope:

$$\begin{cases} T_p(A)_{t=0} = 0. \\ T_p(A)_{t=10^{-3}} = 100. \end{cases}$$

2 Reference solution

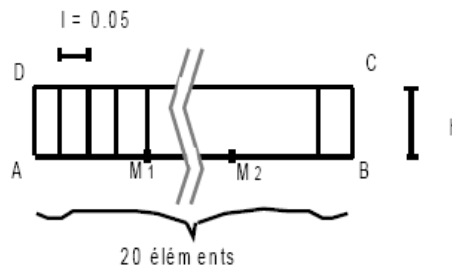
2.1 Method of calculating used for the reference solution

$$\frac{T(x, t) - T_p}{T_0 - T_p} = \frac{4}{\pi} \sum_{n=1}^{\infty} \frac{1}{n} \sin\left(\frac{n\pi x}{2L}\right) \exp\left[-\left(\frac{n\pi}{2L}\right)^2 \cdot \frac{\lambda}{\rho C_p} \cdot t\right]$$

$x =$ X-coordinate

$t =$ Time

$T_0 =$



points	nœuds
M1	N9
M2	N33

$T_p =$ Initial temperature

$T_p =$ Imposed temperature

$n =$ 1,3,5, ...

2.2 Results of reference

Temperatures at the points $M1$ ($x=0.2$) and $M2$ ($x=0.8$), and at various moments ($t=0.1, 0.2, 0.7$ and 2.0).

The values of reference are those given in guide VPCS.

2.3 Uncertainty on the solution

Digital series.

2.4 Bibliographical references

- J.F. SACCADURA: Initiation with the heat transfers, Paris, Technique and documentation (1982).

3 Modeling A

3.1 Characteristics of modeling

QUAD8

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height $h=1.0$ with only one elements sleep.

Limiting conditions:

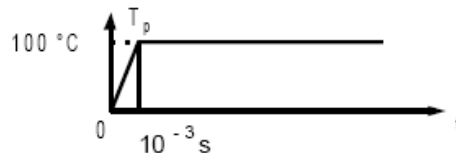
On $[BC]$, $[AB]$ and $[DC]$: $j=0$

on $[AD]$: T_p is imposed

Initial conditions:

$$T=0.^\circ C$$

One fixes here the duration of the shock at 10^{-3}_s



3.2 Characteristics of the grid

Many nodes: 103

Many meshes and types: 20 QUAD8

4 Results of modeling A

4.1 Values tested

Identification	Reference	% difference
<i>M1(x=0.2)N9</i>		
$t=0.1$	65.48	- 0.28
$t=0.2$	75.58	+0.31
$t=0.7$	93.01	- 0.15
$t=2.0$	99.72	- 0.02
<i>M2(x=0.8)N33</i>		
$t=0.1$	8.09	- 0.67
$t=0.2$	26.37	- 2.20
$t=0.7$	78.47	- 0.54
$t=2.0$	99.13	- 0.05

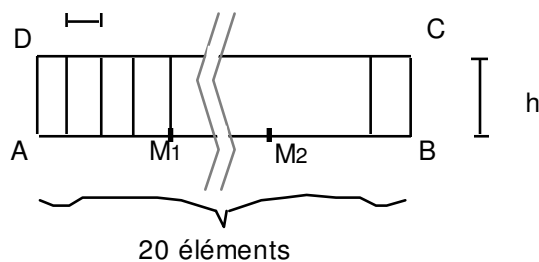
5 Modeling B

5.1 Characteristics of modeling

QUAD8

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height $h = 1.0$ with only one elements sleep.

$$l = 0.05$$

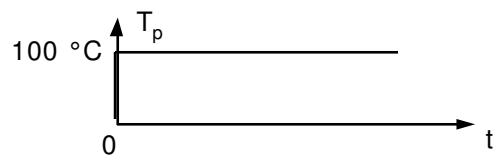


points	nœuds
M1	N9
M2	N33

Conditions limites

sur [BC], [AB] et [DC] $\varphi = 0$

sur [AD] : T_p est imposée $T_p = 100^\circ\text{C}$



Conditions initiales

On affecte directement la température de 100°C à l'instant 0.

5.2 Characteristics of the grid

Many nodes: 103

Many meshes and types: 20 QUAD8

6 Results of modeling B

6.1 Values tested

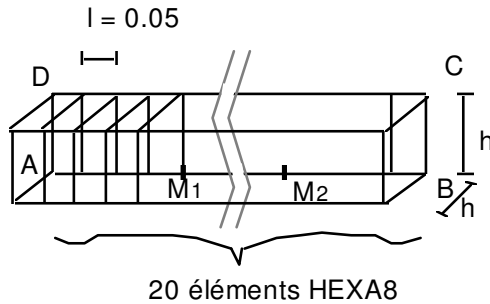
Identification	Reference	% difference
<i>MI(x=0.2) N9</i>		
$t=0.1$	65.48	- 0.17
$t=0.2$	75.58	0.35
$t=0.7$	93.01	- 0.14
$t=2.0$	99.72	- 0.02
<i>M2(x=0.8) N33</i>		
$t=0.1$	8.09	0.28
$t=0.2$	26.37	- 1.89
$t=0.7$	78.47	- 0.51
$t=2.0$	99.13	- 0.05

7 Modeling C

7.1 Characteristics of modeling

HEXA8

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height and a thickness $h = 1.0$ with only one elements sleep.

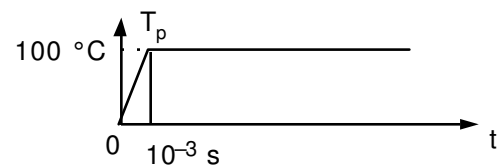


points	nœuds
M1	N21 à N24
M2	N69 à N72

Conditions limites

sur [BC], [AB] et [DC] : $\phi = 0$

sur [AD] : T_p est imposée



Conditions initiales

$T = 0\text{ °C}$

On fixe ici la durée du choc à 10^{-3} s.

7.2 Characteristics of the grid

Many nodes: 84

Many meshes and types: 20 HEXA8

8 Results of modeling C

8.1 Values tested

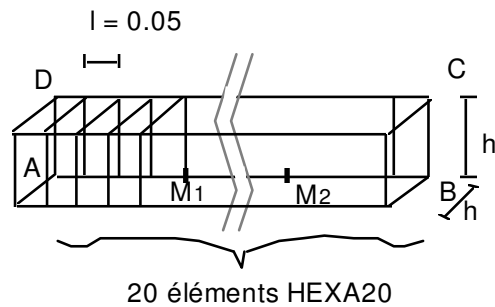
Identification	Reference	% difference
<i>M1(x=0.2) N21</i>		
$t=0.1$	65.48	- 0.26
$t=0.2$	75.58	+0.31
$t=0.7$	93.01	- 0.15
$t=2.0$	99.72	- 0.02
<i>M2(x=0.8) N69</i>		
$t=0.1$	8.09	- 1.31
$t=0.2$	26.37	- 2.30
$t=0.7$	78.47	- 0.53
$t=2.0$	99.13	- 0.05

9 Modeling D

9.1 Characteristics of modeling

HEXA20

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height and a thickness $h = 1.0$ with only one lay down elements.

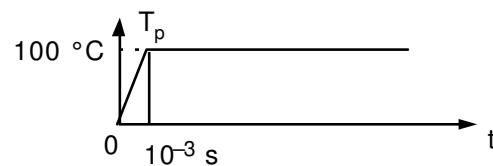


points	nœuds
M1	N57 à N64
M2	N201 à N208

Conditions limites

sur [BC], [AB] et [DC] : $\phi = 0$

sur [AD] : T_p est imposée



Conditions initiales

$T = 0^\circ\text{C}$

On fixe ici la durée du choc à 10^{-3} s.

9.2 Characteristics of the grid

Many nodes: 248

Many meshes and types: 20 HEXA20

10 Results of modeling D

10.1 Values tested

Identification	Reference	% difference
<i>M1(x=0.2) N57</i>		
$t=0.1$	65.48	- 0.28
$t=0.2$	75.58	+0.31
$t=0.7$	93.01	- 0.15
$t=2.0$	99.72	- 0.02
<i>M2(x=0.8) N201</i>		
$t=0.1$	8.09	- 0.67
$t=0.2$	26.37	- 2.20
$t=0.7$	78.47	- 0.54
$t=2.0$	99.13	- 0.05

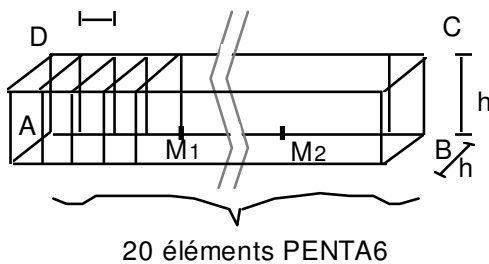
11 Modeling E

11.1 Characteristics of modeling

PENTA6

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height and a thickness $H = 1.0$ with only one lay down elements. Each cube is cut out in 2 pentahedrons.

$$l = 0.05$$

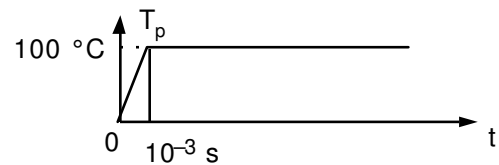


points	nœuds
M1	N21 à N24
M2	N69 à N72

Conditions limites

sur [BC], [AB] et [DC] : $\phi = 0$

sur [AD] : T_p est imposée



Conditions initiales

$T = 0^\circ\text{C}$

On fixe ici la durée du choc à 10^{-3} s.

11.2 Characteristics of the grid

Many nodes: 84

Many meshes and types: 40 PENTA6

12 Results of modeling E

12.1 Values tested

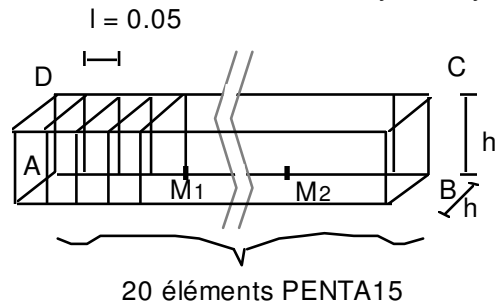
Identification	Reference	% difference
<i>M1(x=0.2) N21</i>		
$t=0.1$	65.48	- 0.26
$t=0.2$	75.58	+0.31
$t=0.7$	93.01	- 0.15
$t=2.0$	99.72	- 0.02
<i>M2(x=0.8) N69</i>		
$t=0.1$	8.09	- 1.31
$t=0.2$	26.37	- 2.30
$t=0.7$	78.47	- 0.53
$t=2.0$	99.13	- 0.05

13 Modeling F

13.1 Characteristics of modeling

PENTA15

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height and a thickness $H = 1.0$ with only one lay down elements. Each cube is cut out in 2 pentahedrons.

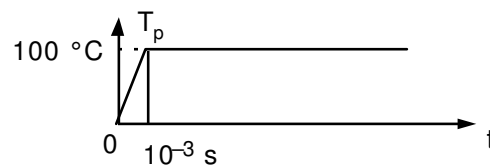


points	nœuds
M1	N62 à N70
M2	N218 à N226

Conditions limites

sur [BC], [AB] et [DC] : $\phi = 0$

sur [AD] : T_p est imposée



Conditions initiales

$T = 0^\circ\text{C}$

On fixe ici la durée du choc à 10⁶ s.

13.2 Characteristics of the grid

Many nodes: 269

Many meshes and types: 40 PENTA15

14 Results of modeling F

14.1 Values tested

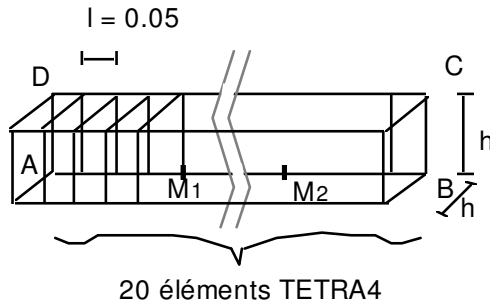
Identification	Reference	% difference
<i>M1(x=0.2) N62</i>		
$t=0.1$	65.48	- 0.28
$t=0.2$	75.58	+0.31
$t=0.7$	93.01	- 0.15
$t=2.0$	99.72	- 0.02
<i>M2(x=0.8) N218</i>		
$t=0.1$	8.09	- 0.67
$t=0.2$	26.37	- 2.20
$t=0.7$	78.47	- 0.54
$t=2.0$	99.13	- 0.05

15 Modeling G

15.1 Characteristics of modeling

TETRA4

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height and a thickness $h = 1.0$ with only one elements sleep. Each cube is cut out in 5 tetrahedrons.

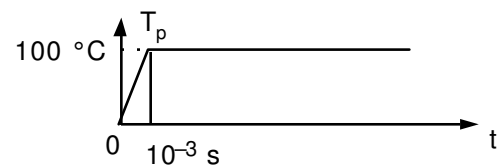


points	nœuds
M1	N12, N17
M2	N48, N53

Conditions limites

sur [BC], [AB] et [DC] : $\phi = 0$

sur [AD] : T_p est imposée



Conditions initiales

$T = 0^\circ\text{C}$

On fixe ici la durée du choc à 10^{-3} s.

15.2 Characteristics of the grid

Many nodes: 84

Many meshes and types: 100 TETRA4

16 Results of modeling G

16.1 Values tested

Identification	Reference	% difference
<i>M1(x=0.2)</i>		
T = 0.1 N12	65.48	- 0.17
N17	65.49	- 0.33
T = 0.2 N12	75.58	+0.34
N17	75.58	+0.29
T = 0.7 N12	93.01	- 0.14
N17	93.01	- 0.16
T = 2.0 N12	99.72	- 0.02
N17	99.72	- 0.02
<i>M2(x=0.8)</i>		
T = 0.1 N48	8.09	- 0.11
N53	8.09	- 1.43
T = 0.2 N48	26.37	- 1.96
N53	26.37	- 2.39
T = 0.7 N48	78.47	- 0.51
N53	78.47	- 0.55
T = 2.0 N48	99.13	- 0.05
N53	99.13	- 0.05

16.2 Remarks

At the beginning of transient, one observes slightly different values between the nodes located in a plan $x = \text{constante}$ (< 3 pour 1000). This anomaly seems to be due to modeling in tetrahedrons with 4 nodes. The results remain nevertheless correct compared to the other elements 3D.

Warning : The translation process used on this website is a "Machine Translation". It may be imprecise and inaccurate in whole or in part and is provided as a convenience.

Copyright 2019 EDF R&D - Licensed under the terms of the GNU FDL (<http://www.gnu.org/copyleft/fdl.html>)

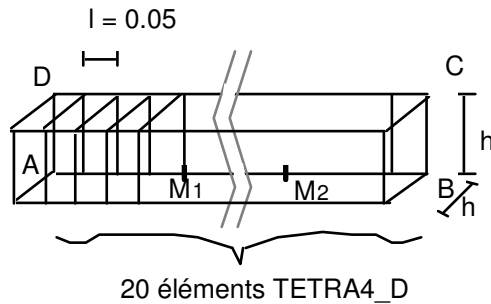
17 Modeling J

17.1 Characteristics of modeling

TETRA4_D

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height and a thickness $h = 1.0$ with only one elements sleep. Each cube is cut out in 5 tetrahedrons.

Modeling is used 3D_DIAG applied to TETRA4, which corresponds to the lumpage of the matrix of thermal mass.

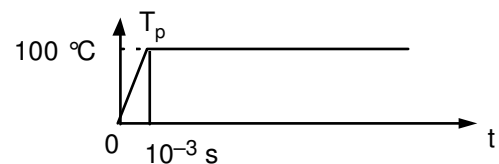


points	nœuds
M1	N12, N17
M2	N48, N53

Conditions limites

sur [BC], [AB] et [DC] : $\phi = 0$

sur [AD] : T_p est imposée



Conditions initiales

$T = 0\text{ °C}$

On fixe ici la durée du choc à 10^{-3} s.

17.2 Characteristics of the grid

Many nodes: 84

Many meshes and types: 100 TETRA4

18 Results of modeling J

18.1 Values tested

Identification	Reference	% difference
<i>M1(x=0.2)</i>		
T = 0.1 N12	65.48	- 0.21
N17	65.49	- 0.36
T = 0.2 N12	75.58	+0.34
N17	75.58	+0.29
T = 0.7 N12	93.01	- 0.15
N17	93.01	- 0.16
T = 2.0 N12	99.72	- 0.02
N17	99.72	- 0.02
<i>M2(x=0.8)</i>		
T = 0.1 N48	8.09	+1.16
N53	8.09	- 0.15
T = 0.2 N48	26.37	- 1.77
N53	26.37	- 2.20
T = 0.7 N48	78.47	- 0.52
N53	78.47	- 0.57
T = 2.0 N48	99.13	- 0.05
N53	99.13	- 0.05

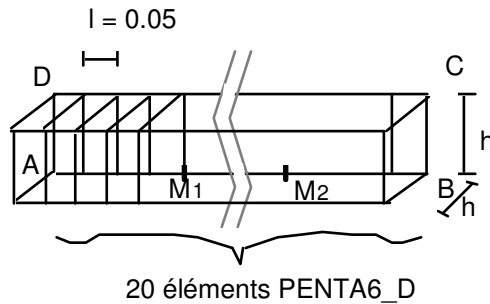
19 Modeling K

19.1 Characteristics of modeling

PENTA6_D

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height and a thickness $h = 1.0$ with only one elements sleep. Each cube is cut out in 2 pentahedrons.

Modeling is used 3D_DIAG applied to PENTA6, which corresponds to the lumpage of the matrix of thermal mass.

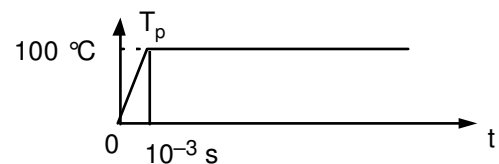


points	nœuds
M1	N21 à N24
M2	N69 à N72

Conditions limites

sur [BC], [AB] et [DC] : $\phi = 0$

sur [AD] : T_p est imposée



Conditions initiales

$T = 0^\circ\text{C}$

On fixe ici la durée du choc à 10^{-3} s.

19.2 Characteristics of the grid

Many nodes: 84

Many meshes and types: 40 PENTA6

20 Results of modeling K

20.1 Values tested

Identification	Reference	% difference
$M1(x=0.2)$		
$t=0.1$	65.48	- 0.30
$t=0.2$	75.58	+0.31
$t=0.7$	93.01	- 0.15
$t=2.0$	99.72	- 0.02
$M2(x=0.8)$		
$t=0.1$	8.09	- 0.03
$t=0.2$	26.37	- 2.14
$t=0.7$	78.47	- 0.55
$t=2.0$	99.13	- 0.05

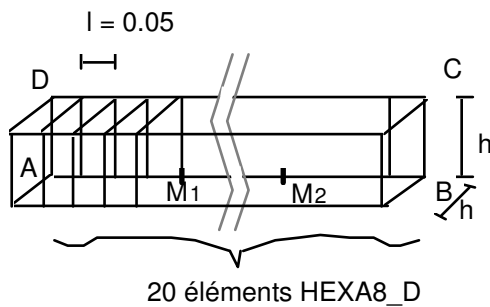
21 Modeling L

21.1 Characteristics of modeling

HEXA8_D

One nets only half the thickness of the wall by reason of symmetry; modeling is made under a height and a thickness $h = 1.0$ with only one elements sleep.

Modeling is used 3D_DIAG applied to HEXA8, which corresponds to the lumpage of the matrix of thermal mass.

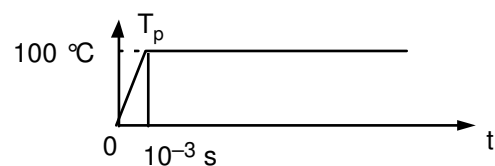


points	nœuds
M1	N21 à N24
M2	N69 à N72

Conditions limites

sur [BC], [AB] et [DC] : $\phi = 0$

sur [AD] : T_p est imposée



Conditions initiales

$T = 0^\circ\text{C}$

On fixe ici la durée du choc à 10^{-3} s.

21.2 Characteristics of the grid

Many nodes: 84

Many meshes and types: 20 HEXA8

22 Results of modeling L

22.1 Values tested

Identification	Reference	% difference
<i>M1(x=0.2)</i>		
$t=0.1$	65.48	- 0.30
$t=0.2$	75.58	+0.31
$t=0.7$	93.01	- 0.15
$t=2.0$	99.72	- 0.02
<i>M2(x=0.8)</i>		
$t=0.1$	8.09	- 0.03
$t=0.2$	26.37	- 2.10
$t=0.7$	78.47	- 0.55
$t=2.0$	99.13	- 0.05

23 Summary of the results

At the end of 0.7 S the error is definitely lower than 1% for the various thermal elements 2D (QUAD8) and 3D (HEXA8 - HEXA20 - PENTA6 - PENTA15 - TETRA4) used.

It does not seem that the lumpage improves the digital result.

It would be advisable to test the elements lumpés with a true jump as in modeling B.