

## TTLV300 - Parallelepiped subjected to a density flux on its faces

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### Summary:

This test is resulting from the validation independent of version 3 in linear transitory thermics.

It is about a voluminal problem represented by a modeling 3D.

The features tested are the following ones:

- voluminal thermal element,
- transitory algorithm of thermics,
- limiting conditions: imposed flow.

The results are compared with a three-dimensional analytical solution.

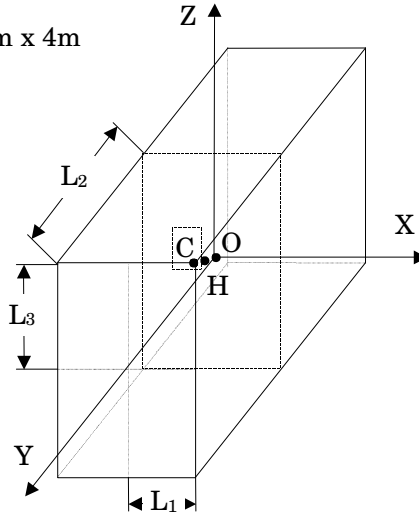
## 1 Problem of reference

### 1.1 Geometry

Dimensions du parallélépipède: 2m x 3.2m x 4m

- $L_1 = 1.0$  m
- $L_2 = 1.6$  m
- $L_3 = 2.0$  m

Point O (0.,0.,0.)  
Point H (0.5,0.8,1.0)  
Point C (1.0,1.6,2.0)



### 1.2 Properties of material

$\lambda = 1. W/m^{\circ}C$	thermal conductivity
$c_p = 1. J/kg^{\circ}C$	specific heat
$\rho = 1. kg/m^3$	density

### 1.3 Boundary conditions and loadings

Flow imposed on the 6 faces  $q = 0.5 W/m^2 = q_w$

### 1.4 Initial conditions

$T(t=0) = 1^{\circ}C = T_0$

## 2 Reference solution

### 2.1 Method of calculating used for the reference solution

$T(x, y, z, t) = T_0 + 2q_w \frac{\sqrt{\alpha t}}{\lambda} (A + B + C)$  with:

$$A = \sum_{m=0}^{\infty} \left[ i.erfc \left[ \frac{(2m-1)L_1 + x}{2\sqrt{\alpha t}} \right] + i.erfc \left[ \frac{(2m-1)L_1 - x}{2\sqrt{\alpha t}} \right] \right]$$

$$B = \sum_{m=0}^{\infty} \left[ i.erfc \left[ \frac{(2m-1)L_2 + y}{2\sqrt{\alpha t}} \right] + i.erfc \left[ \frac{(2m-1)L_2 - y}{2\sqrt{\alpha t}} \right] \right]$$

$$C = \sum_{m=0}^{\infty} \left[ i.erfc \left[ \frac{(2m-1)L_3 + z}{2\sqrt{\alpha t}} \right] + i.erfc \left[ \frac{(2m-1)L_3 - z}{2\sqrt{\alpha t}} \right] \right]$$

$$\alpha = \frac{\lambda}{\rho C_p}$$

The values of reference are obtained with  $m = 1000$ .

### 2.2 Results of reference

Temperature at the points:  $O(0,0,0)$ ,  $H(0.5,0.8,1.)$  and  $C(1.,1.6,2.)$

### 2.3 Uncertainty on the solution

Analytical solution.

### 2.4 Bibliographical references

- M.J Chang, L.C Chow, W.S Chang, "Improved alternating direction implicit for solving transient three dimensional heat diffusion problems", Numerical Heat Transfer, flight 19, pp 69-84, 1991.

## 3 Modeling A

### 3.1 Characteristics of modeling

3D (HEXA8, PENTA6)

Modélisation 1/8 du parallélépipède

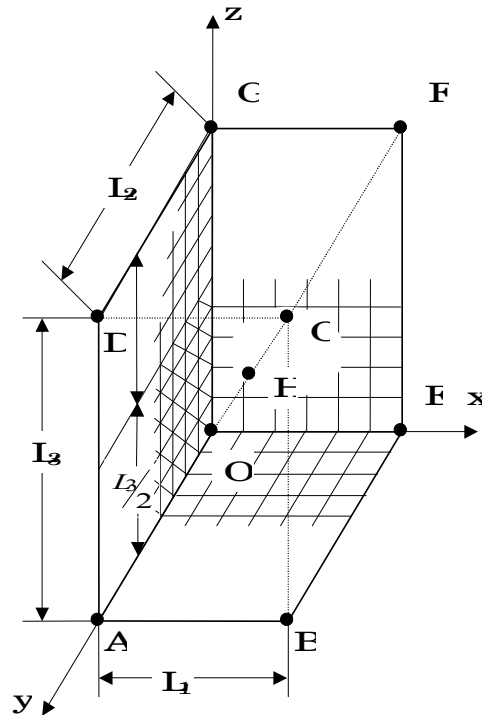
Maillage

- 6 éléments suivant x
- 8 éléments suivant y
- 10 éléments suivant z

Conditions limites

- faces [ABCD], [BEFC], [DEFG]:  $q_v = 0.5$
- faces [ABFC], [ACGD], [CEFG]:  $\phi = 0$

Points	x	y	z	Nœud
O	000	000	000	N2
H	050	08	100	N109
C	100	16	200	N814



### 3.2 Characteristics of the grid

Many nodes: 819  
Many meshes and types: 288 HEXA8, 576 PENTA6 (168 QUAD4, 96 TRIA3)

### 3.3 Remarks

The limiting condition  $\phi = 0$  is implicit on the free edges.

Discretization of time: 36 intervals, enters 0.s and 10.s (of 0.005.s with 1.s by interval).

## 4 Results of modeling A

### 4.1 Values tested

Identification	Reference	Aster	% difference	Tolerance
Not O				
(N2) T = 0.05 S	1.0001	1.00000443	-0,010	1%
T = 0.1 S	1.00398	1.003172	-0,080	1%
T = 0.2 S	1.03331	1.03127	-0,198	1%
T = 0.3 S	1.08533	1.08227	-0,282	1%
T = 0.5 S	1.23086	1.2266	-0,345	1%
T = 1. S	1.69979	1.6945	-0,311	1%
T = 5. S	5.9292	5.9234	-0,098	1%
T = 10. S	11,242	11,236	-0,054	1%
Not H				
(N409) T = 0.05 S	1.0083	1.006472	-0,181	1%
T = 0.1 S	1.03819	1.03573	-0,237	1%
T = 0.2 S	1.12556	1.1229	-0,235	1%
T = 0.3 S	1.22594	1.2233	-0,217	1%
T = 0.5 S	1.43580	1.4331	-0,188	1%
T = 1. S	1.96667	1.9639	-0,140	1%
T = 5. S	6.2167	6.2139	-0,045	1%
T = 10. S	11,529	11,526	-0,023	1%
Not C				
(N814) T = 0.05 S	1.3785	1.3726	-0,429	1%
T = 0.1 S	1.5352	1.5308	-0,290	1%
T = 0.2 S	1.7572	1.7536	-0,206	1%
T = 0.3 S	1.9295	1.9261	-0,176	1%
T = 0.5 S	2.2142	2.2110	-0,146	1%
T = 1. S	2.8085	2.8054	-0,112	1%
T = 5. S	7.0792	7.0762	-0,043	1%
T = 10. S	12,392	12,389	-0,027	1%

## 5 Summary of the results

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The got results are satisfactory. The maximum change (0.43%), is located on surface external of the parallelepiped (Not  $C$ ) at the moment  $t$  weakest. At the end of  $10 s$ , this variation decreases, the maximum is then of 0,054% (not  $O$  : center of the parallelepiped).

This test made it possible to test in linear transient modeling 3D with meshes HEXA8 and PENTA6.