

## PLEXU04: Cylinder with cables of prestressed under internal pressure in transitory dynamics

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### Summary:

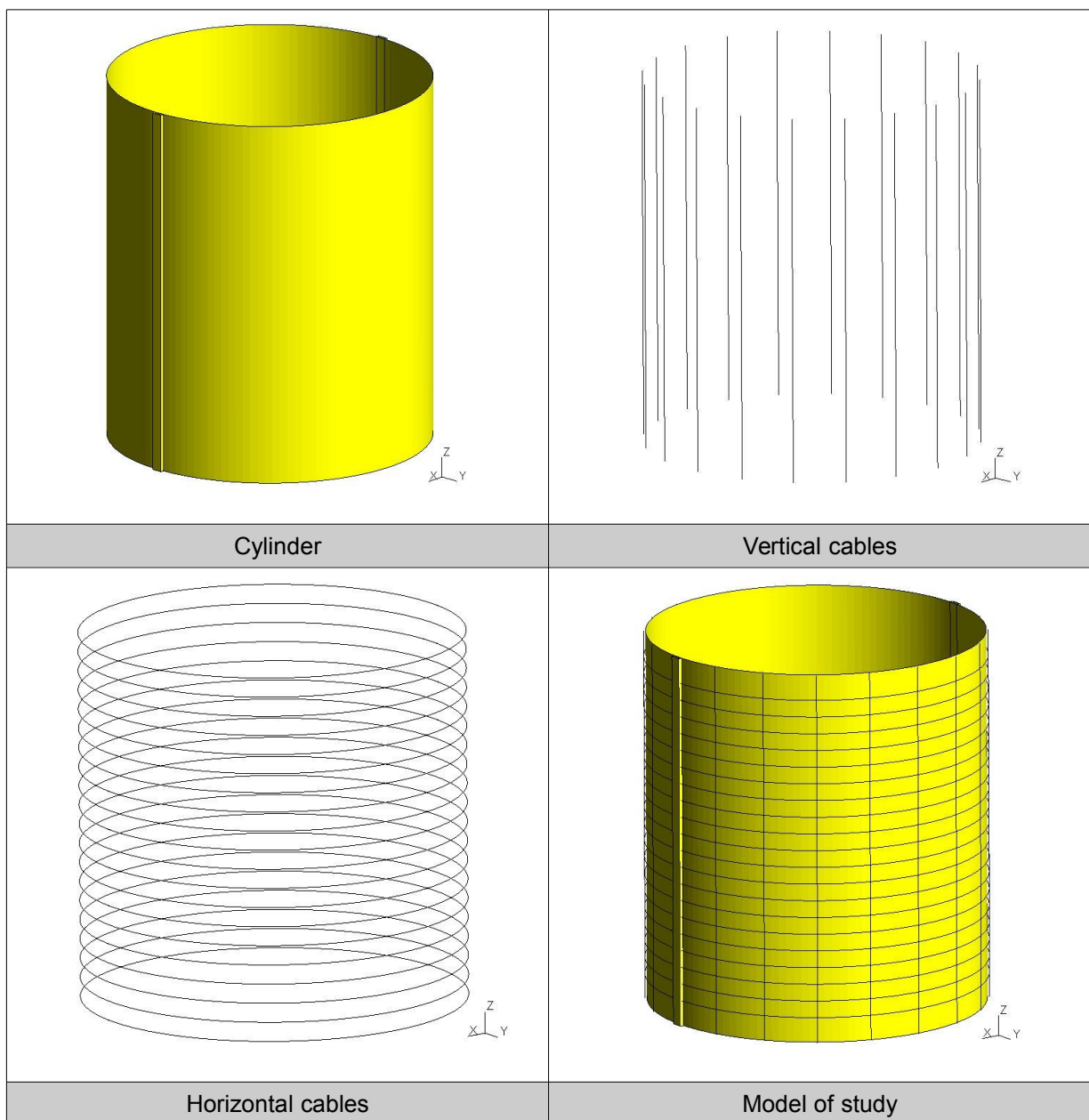
The purpose of this test is of valider all the features installation within the framework of the methodology of Code\_Aster/Europlexus chaining for the use of prestressing in Europlexus, on a semi-industrial model (these features having been tested, together and/or separately, only on elementary tests).

For that, one compares the results resulting from the macro-order `CALC_EUROPLEXUS` with those resulting from the operator `DYNA_NON_LINE` using the explicit diagram of the differences finished .

## 1 Description

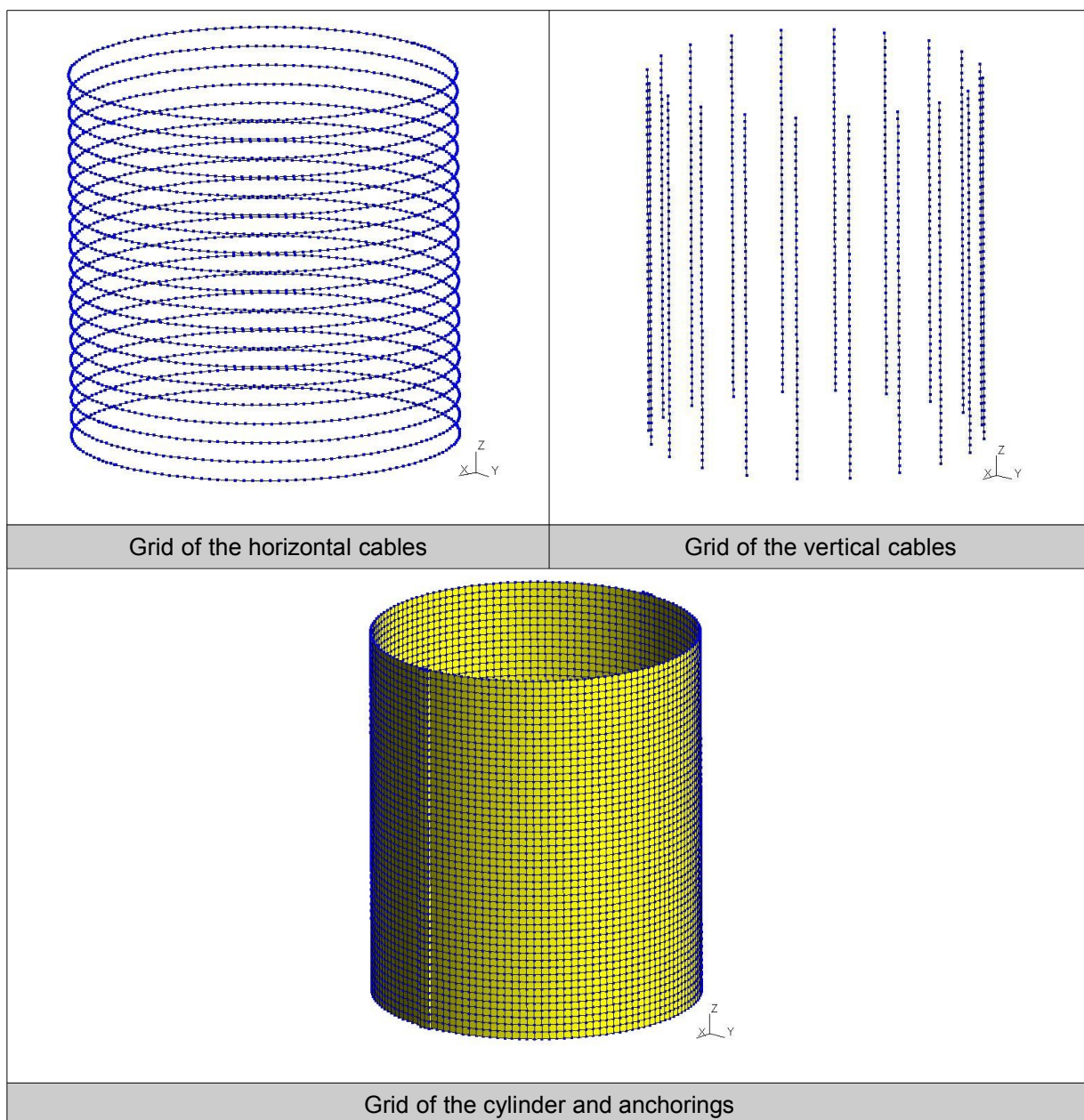
### 1.1 Geometry

The model of study is a cylindrical envelope of average radius  $R=21.9\text{ m}$  , height  $H=49.6\text{ m}$  and thickness  $t=0.6\text{ m}$  . Anchorings for the cables on the sides of the cylinder, have as a length  $L=1.5\text{ m}$  and for width  $l=0.5\text{ m}$  . Concerning the cables, they are positioned on the skin external of the cylinder. They are then offset of a distance  $e=0.25\text{ m}$  . The model is composed of 20 horizontal cables and of 20 vertical cables. The figures below present the various components of the model of study.



## 1.2 Grid

The cables are with a grid with meshes `SEG2`. The cylinder and anchorings for the cables are with a grid with meshes `QUAD4`. The discretization spaces some for the various components is to the maximum of  $f = 1.0 m$ . The following figures represent the grids for the various parts of the model.



## 1.3 Properties of materials

The properties of the concrete for the cylinder and anchorings and of steel for the cables of prestressing are indexed in the following table.

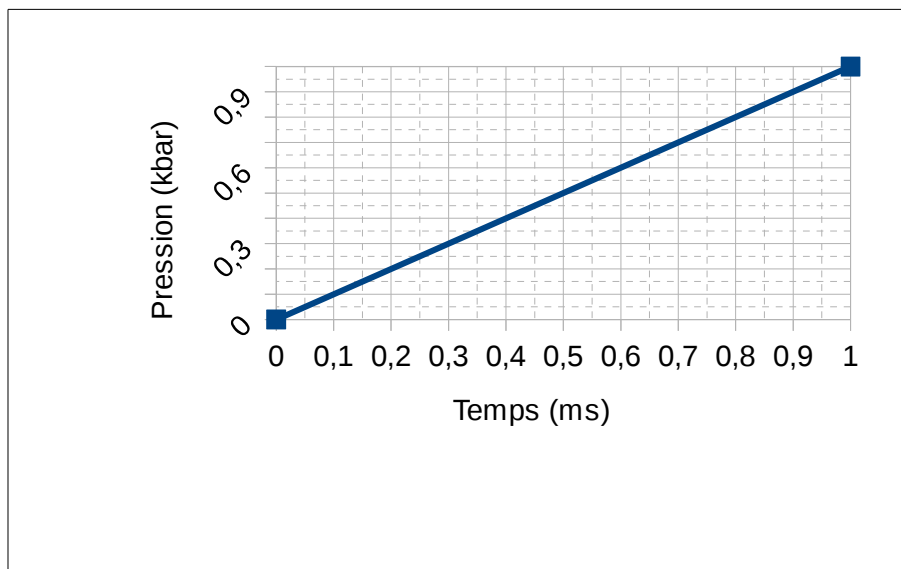
Material	Concrete	Steel
Young modulus	$4 \times 10^{10} Pa$	$1.93 \times 10^{11} Pa$
Poisson's ratio	0.2	0.0
Density	$2500 kg/m^3$	$7850 kg/m^3$
Elastic ultimate stress	<i>n/a</i>	$1.94 \times 10^{11} Pa$

## 1.4 Boundary conditions and loadings

The cylinder and anchorings are embedded in top and bottom.

One initially imposes a tension in the cables equalizes with  $3.75 \times 10^6 N$ . The nodes at the ends of the vertical and horizontal cables are considered "active".

In the second time, one subjects the cylinder to an internal pressure which increases in the course of time (  $P_i=0 Pa$  with  $P_f=1 kbar$  in  $\Delta t=1 ms$  ). This loading is represented on the following graph.



## 1.5 Principal stages of the tests

The macro-order is used `DEFI_CABLE_BP` to obtain the relations kinematics between the cylinder and the cables as well as the loading related to the tension in the cables.

One launches then the macro-order `CALC_PRECONT` to carry out the setting into prestressed structure starting from the tensions of the cables given.

The result of this setting in prestressing is given in initial state to the macro-order `CALC_EUROPLEXUS` in order to calculate the mechanical response of the cylinder prestressed to the internal loading of pressure.

To validate the results resulting from `CALC_EUROPLEXUS`, one does the same calculation with the operator `DYNA_NON_LINE`.

From the two concept-results obtained, one extracts:

- the evolution according to the time of displacement on the point of reference located at the middle height of the cylinder, is in  $(0, R, H/2)$ , noted  $N_{ref}^{cyl}$ .
- efforts resulting from membrane  $N_{xx}$  and  $N_{yy}$ , at three moments different in a mesh from the cylinder having a node in common with the node of reference of the cylinder, noted  $M_{ref}^{cyl}$ .
- normal effort in an element of the readiest horizontal cable localised of the middle height of the cylinder and more far from anchorings, noted  $EL_{ref}^{cab}$ .

## 2 Reference solution

### 2.1 Results of reference

The results of reference are those obtained with `DYNA_NON_LINE`.

### 2.2 Uncertainty on the solution

Inaccuracies of `DYNA_NON_LINE`.

### 3 Modeling A

The modeling of hulls proposed is Q4GG. The steel wire ropes are modelled by elements BAR.

The step of time used for calculations is of  $\Delta t = 0.1 \mu s$ , he observes the stability condition (condition CFL).

#### 3.1 Sizes tested and results

The component is tested *DY* displacement with the node  $N_{ref}^{cyl}$  at three different moments.

Node	Component	Moment (ms)	Value of reference (m)	Tolerance (%)
$N_{ref}^{cyl}$	<i>DY</i>	0	-0.00149171629532	1.E-6
$N_{ref}^{cyl}$	<i>DY</i>	0,5	-0.000144254069992	1.0
$N_{ref}^{cyl}$	<i>DY</i>	1	0.00927115873819	0.3

One tests the value of two components of the generalized efforts  $N_{xx}$  and  $N_{yy}$ , in the mesh  $M_{ref}^{cyl}$  at three different moments.

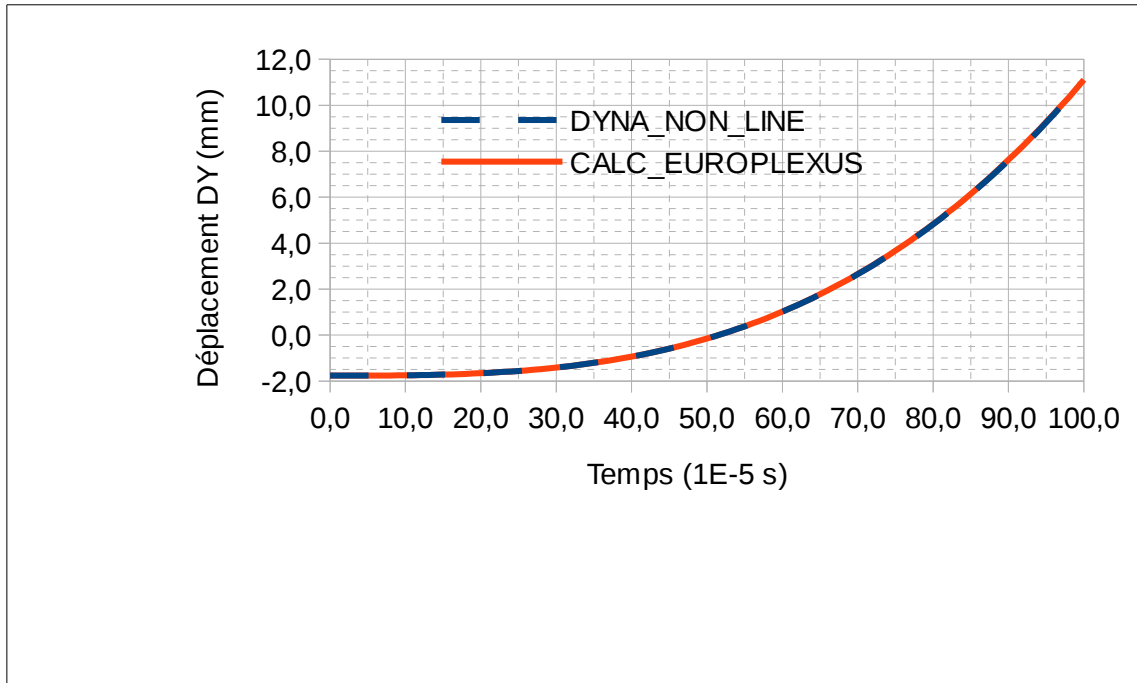
Mesh	Component	Moment (ms)	Value of reference (NR)	Tolerance (%)
$M_{ref}^{cyl}$	$N_{xx}$	0	-298115.503936	1.0E-6
$M_{ref}^{cyl}$	$N_{xx}$	0,5	12143.207589	9,0
$M_{ref}^{cyl}$	$N_{xx}$	1	2183571.35963	0.25

Mesh	Component	Moment (ms)	Value of reference (NR)	Tolerance (%)
$M_{ref}^{cyl}$	$N_{yy}$	0	-1671586.18169	1.0E-6
$M_{ref}^{cyl}$	$N_{yy}$	0,5	-115744.270149	0.5
$M_{ref}^{cyl}$	$N_{yy}$	1	10770364.4408	0.03

One tests the value of normal effort, in the element  $EL_{ref}^{cab}$  at three different moments.

Mesh	Component	Moment (ms)	Value of reference (NR)	Tolerance (%)
$EL_{ref}^{cab}$	$N$	0	3750000.0	2.0E-3
$EL_{ref}^{cab}$	$N$	0,5	3808797.87598	0.2
$EL_{ref}^{cab}$	$N$	1	4229204.64926	0.5

The graph below trace the evolution of the displacement of the point of reference obtained is with the order DYNA\_NON\_LINE, that is to say with CALC\_EUROPLEXUS.



## 4 Synthesis

The tests carried out on the most important sizes of the model show that the computed values with CALC\_EUROPLEXUS are very close to those obtained with DYNA\_NON\_LINE.

Within sight of the graph on the evolution of displacement  $DY$  point of reference of the cylinder according to time, one notes first of all that prestressing was indeed taken into account, because initial displacement is negative, and thereafter that the two curves are superimposed.

It is concluded that the vertical and horizontal cables as well as the relations kinematics were correctly defined and taken into account during dynamic calculation with the order CALC\_EUROPLEXUS, since this order is able correctly to restore the value of displacements, the efforts generalized in the hulls and the efforts in the cables after application of a loading in dynamics.