

## SSNA103 - Chock of the parameters of the model of Weibull

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### Summary:

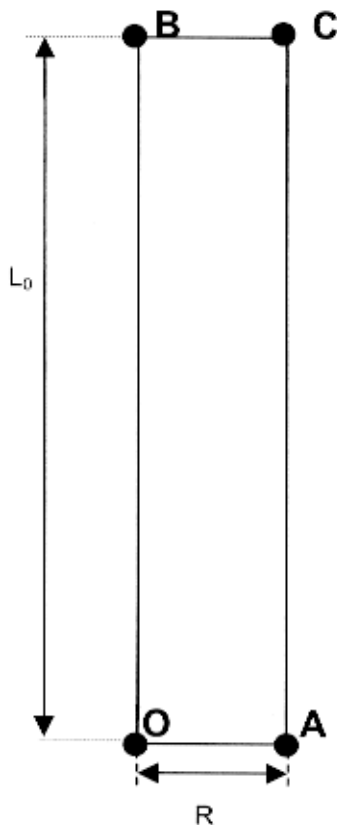
This test validates the order RECA\_WEIBULL allowing the identification of the parameters  $m$  and  $\sigma_u$  model of Weibull.

The identification is carried out using a database made up of 45 tests, all carried out on smooth cylindrical test-tubes at three different temperatures,  $-150^{\circ}C$ ,  $-100^{\circ}C$  and  $-50^{\circ}C$ . This database is obtained by random pulling of a representative sample of the statistical law of Weibull corresponding to values of  $m$  and  $\sigma_u$  fixed arbitrarily.

## 1 Problem of reference

### 1.1 Geometry

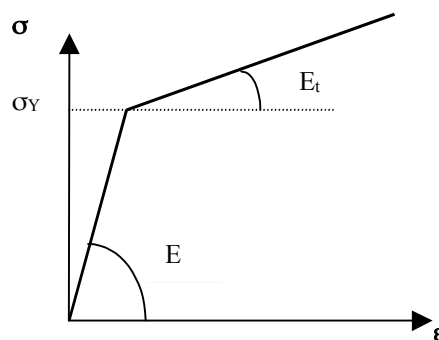
Each test is carried out on a smooth cylindrical test-tube. For obvious reasons of symmetries, an axisymmetric modeling 2D of the quarter of the structure is sufficient.



Rayon de l'éprouvette :  $R = 68 \text{ mm}$ .  
Demi-longueur de référence pour la mesure de l'élongation :  $L_0 = 203,5 \text{ mm}$

### 1.2 Properties of material

One describes the behavior of material studied by an elastoplastic law of Von Mises with linear isotropic work hardening, 'VMIS\_ISOT\_LINE'. The deformations used in the relation of behavior are the linearized deformations.



The Poisson's ratio does not depend on the temperature,  $\nu = 0,3$ .

Values of the Young modulus  $E$ , tangent module  $E_t$ , and of the elastic limit are given in the following table:

Temperature [ $^{\circ}C$ ]	- 150	- 100	- 50
$E [MPa]$	200000	200000	200000
$E_t [MPa]$	2000	2000	2000
$\sigma_y [MPa]$	750	700	650

## 1.3 Boundary conditions and loadings

By referring to the figure of the §1.1 the boundary conditions and loadings are the following:

On the segment  $BC$  ( $Y=L_0$ ), imposed displacement following the direction  $OY$ :

$T [^{\circ}C]$       Displacement ( $l-l_0$ ) with the rupture for a reference length  $l_0$  of 203.5 mm  
[mm]

The results for each temperature are classified by ascending order

<b>-50</b>	10.68	28.78	30.31	31.66	32.53	33.90	34.38	35.82	36.69	37.09	37.37	37.49	38.45	39.77	44.39
<b>-100</b>	20.57	21.68	23.32	24.37	24.66	25.59	25.84	27.51	28.44	29.30	29.68	30.16	30.18	30.20	30.95
<b>-150</b>	11.33	14.70	14.79	14.90	18.62	18.87	19.00	19.37	19.61	20.07	21.19	22.79	23.28	24.17	24.41

On the segment  $OA$  ( $Y=0$ ) displacements blocked according to the direction  $OY$ .

On the segment  $OB$  ( $X=0$ ) displacements blocked according to the direction  $OX$ .

## 1.4 Initial conditions

Worthless constraints and deformations.

## 2 Reference solution

### 2.1 Method of calculating

No calculation is necessary to obtain the reference solution. Values  $m$  and  $\sigma_u$  (M and SIGM\_REFE in the option WEIBULL of DEFI\_MATERIAU) that one seeks to identify with Code\_Aster are known and allow to generate the base of the experimental data. Thus, the elongations with rupture are in the following way given:

For each couple  $m$  and  $\sigma_u$  associated with a temperature of test, a sample of 15 values of constraint of Weibull to the rupture were determined by random pulling taking into account the following statistical law:

$$P_f(\sigma_w) = 1 - \exp\left[-\left(\frac{\sigma_w}{\sigma_u}\right)^m\right]$$

The constraint of Weibull is defined by:

$$\sigma_w = \sqrt[m]{\sum_i (\sigma_i^i)^m \frac{V_i}{V_0}}$$

The summation relates to volumes of matter  $V_i$  plasticized,  $\sigma_i^i$  indicating the maximum principal constraint in each one of these volumes (volume  $V_0$  (VOLU\_REFE in the option WEIBULL of DEFI\_MATERIAU) is equal to  $(50 \mu m^3)$ ).

In the case of a request in simple traction with the assumption of the small deformations, the constraint of Weibull,  $\sigma_w$ , expresses itself according to the elongation with the rupture  $(l-l_0)/l_0$ , according to:

$$\sigma_w = E_t \frac{l-l_0}{l_0} + \left[1 - \frac{E_t}{E} \sigma_y\right]^m \sqrt[m]{\frac{V}{V_0}}$$

One thus deduces from this expression and preceding random pulling the values of the lengthenings with rupture deferred in the table of [§1.3].

### 2.2 Sizes and results of reference

Reference variables of  $m$  and  $\sigma_u$  used to create the bases of experimental tests are the following ones:

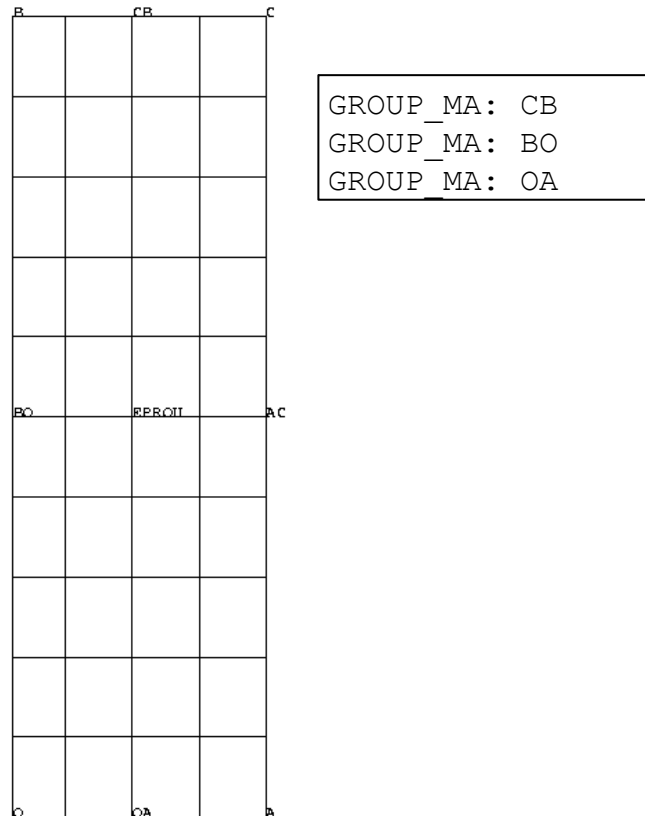
Temperature [°C]	- 50	- 100	- 150
$m$	24	24	24
$\sigma_u$ [MPa]	2800	2700	2600

### 2.3 Uncertainties on the solution

Uncertainty on the solution cannot be given in a precise way. It can be rather high. Indeed, the values of reference can be found only if one considers experimental populations made up of an infinite number of samples.

## 3 Modeling A

### 3.1 Characteristics of the grid



Many nodes: 149  
Many meshes and types: 40 elements QUAD8

### 3.2 Sizes tested and results

Identification of one  $m$  common run at the three experimental bases and of one  $\sigma_u$  by base.

Temperature [ $^{\circ}C$ ]	Reference		Code_Aster	
	$m$	$\sigma_u$ [MPa]	$m$	$\sigma_u$ [MPa]
- 50	24	2800	26.7	2536
- 100	24	2700	26.7	2428
- 150	24	2600	26.7	2372

### 3.3 Remarks

Although the variation enters the values of ( $m$ ,  $\sigma_u$ ) obtained with RECA\_WEIBULL and their values of reference remains considerable, it is in conformity with the result sought taking into account the relatively low number of samples used for retiming (15 per temperature). To obtain the values of reference it would be necessary considerably to increase the number of samples per temperature (

$N > 1000$  ). The noted variation remains however reasonable (about 10%). In addition, growth of  $\sigma_u$  according to the temperature is respected

## 4 Summary of the results

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Results got by *Code\_Aster* show that the automatic procedure of chock of the parameters of the models of Weibull functions and gives coherent results with the expected theoretical results.