

SSNV136 - Triaxial compression test drained with model CJS (level 2)

Summary

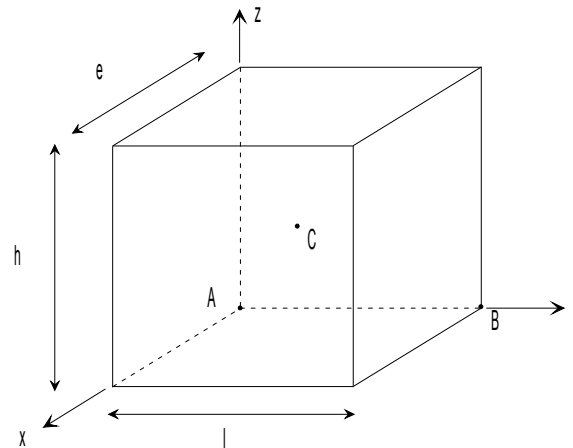
This test makes it possible to validate level 2 of model CJS. It is about a triaxial compression test in drained condition. Calculations are carried out only on the solid part of the ground, without hydraulic coupling. The level of containment is of 100 kPa .

By reason of symmetry, one is interested only in the eighth of a sample 3D subjected to a triaxial compression test.

It is about a test of nonregression. Nevertheless, results got with *Code_Aster* for model CJS2 are compared with those obtained with a private version of the software SPLASH -2D.

1 Problem of reference

1.1 Geometry



height: $h = 1\text{ m}$
width: $l = 1\text{ m}$
thickness: $e = 1\text{ m}$

Coordinates of the points (in meters):

	A	B	C
x	0.	0.	0.5
y	0.	1.	0.5
z	0.	0.	0.5

1.2 Material property

$$E = 35,6616541 \cdot 10^3 \text{ kPa}$$

$$\nu = 0,15037594$$

Parameters CJS2: $\beta = -0,55$ $\gamma = 0,82$ $R_m = 0,289$ $R_c = 0,265$ $n = 0,6$
 $K_o^p = 25,5 \cdot 10^3 \text{ kPa}$ $A = 0,25 \text{ kPa}$ $P_a = -100 \text{ kPa}$

1.3 Initial conditions, boundary conditions, and loading

Phase 1:

One brings the sample in a homogeneous state: $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0$, by imposing the corresponding confining pressure on the front, side right-hand side and higher faces. Displacements are blocked on the faces postpones ($u_x = 0$), side left ($u_y = 0$) and lower ($u_z = 0$).

Phase 2:

One maintains displacements blocked on the faces postpones ($u_x = 0$), side left ($u_y = 0$) and lower ($u_z = 0$), as well as the confining pressure on the front faces and side right-hand side. One applies a displacement imposed to the higher face: $u_z(t)$, in order to obtain a deformation $\varepsilon_{zz} = -20\%$ (counted starting from the beginning of phase 2).

2 Reference solution

2.1 Method of calculating used for the reference solution

The results got with the software a private version of the Flac-2D software are used as reference.

2.2 Results of reference

Constraints σ_{xx} , σ_{yy} and σ_{zz} at the points A , B and C .

2.3 Uncertainty on the solution

Uncertainty related to the Flac-2D software.

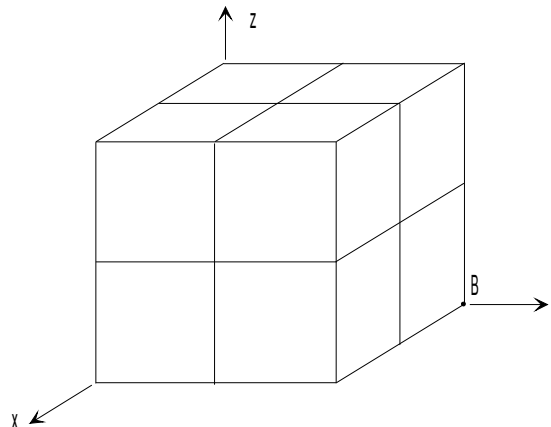
2.4 Bibliography

- 1 Board, "SPLASH (Fast Lagrangian Analysis of Continua) Version 2.20. U.S. NRC", NUREG/CR-5430, October 1989.
- 2 "Splash Fast Lagrangian Analysis of Continua. Theory and Background." Itasca Consulting Group.

3 Modeling A

3.1 Characteristics of modeling

3D:



Cutting: 2 in height, in width and thickness.

Loading of phase 1:

Confining pressure: $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0$: successively -100 kPa , -200 kPa and -400 kPa .

Level 2 of model CJS

3.2 Characteristic of the grid

Many nodes: 27

Many meshes and types: 8 HEXA8 and 24 QUA4

3.3 Values tested

For $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0$: -100 kPa

Localization	Sequenc e number	axial deformation ε_{zz} (%)	constraint (kPa)	Reference
Not A, B and C		- 0.8%	σ_{xx}	- 100.0
		- 20.0%	σ_{xx}	- 100.0
		- 0.8%	σ_{yy}	- 100.0
		- 20.0%	σ_{yy}	- 100.0
		- 0.8%	σ_{zz}	- 286.8
		- 1.6%	σ_{zz}	- 332.9
		- 3.2%	σ_{zz}	- 350.8
		- 7.2%	σ_{zz}	- 356.1
		- 20.0%	σ_{zz}	- 358.8

4 Summary of the results

Values of the constraints obtained with *Aster* coincide with those of the software *SPLASH* with a lower deviation than 0.05%.