

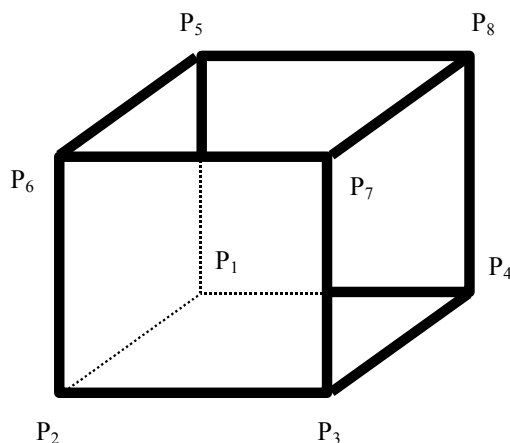
SSNV169 - Coupling creep – damage

Summary:

It is about an elementary test of not-regression making it possible to validate the coupling between the clean model of creep `BETON_UMLV_FP` and models of damage `ENDO_ISOT_BETON` and `MAZARS`. The test consists in maintaining an effort constant on an element and letting it creep.

1 Problem of reference

1.1 Geometry and boundary conditions



Blocages

P1P2P3P4 : $dz=0$

P1P4P8P7 : $dx=0$

P1P2P6P5 : $dy=0$

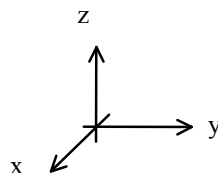
P2P3P7P6 : liaison uniforme suivant x

P3P4P8P7 : liaison uniforme suivant y

Traction

P5P6P7P8 : effort imposé

{dx, dy, dz} sont les déplacements des noeuds suivant les trois directions.



1.2 Properties of material

Two sets of different parameters are used for the coupling with the model ENDO_ISOT_BETON (modeling A, B and C) and for the model of MAZARS (modeling D with I). They are synthesized in the two following tables.

Data materials used for the coupling BETON_UMLV_FP/ENDO_ISOT_BETON

Elastic parameters

E	31 GPa
NAKED	0.2

Parameters of creep

K_RS	$1.2 \cdot 10^5 \text{ MPa}$
ETA_RS	$2.21 \cdot 10^{10} \text{ MPa.s}$
K_IS	$6.22 \cdot 10^4 \text{ MPa}$
ETA_IS	$4.16 \cdot 10^{10} \text{ MPa.s}$
K_RD	$3.86 \cdot 10^4 \text{ MPa}$
ETA_RD	$6.19 \cdot 10^{10} \text{ MPa.s}$
ETA_ID	$1.64 \cdot 10^{12} \text{ MPa.s}$

Parameters of damage

SYT	3 MPa
D_SIGM_EPSI	-6 GPa
SYC	30 MPa

Data materials used for the coupling BETON_UMLV_FP/MAZARS

Elastic parameters

E	31 GPa
NAKED	0.2

Parameters of creep

K_RS	$6.0 \cdot 10^4$ MPa
ETA_RS	$1.0 \cdot 10^{10}$ MPa.s
K_IS	$3.0 \cdot 10^4$ MPa
ETA_IS	$2.4 \cdot 10^{10}$ MPa.s
K_RD	$3.4 \cdot 10^4$ MPa
ETA_RD	$4.08 \cdot 10^{11}$ MPa.s
ETA_ID	$5.44 \cdot 10^{12}$ MPa.s

Parameters of damage

EPSD0	$5.6 \cdot 10^{-5}$
AT	0.831
BT	21 330.
AC	1.15
BC	1390.
K	0.7
CHI	0.6

Parameter not-room

LONG_CARA	0 (100 for the test I)
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It is supposed that drying does not evolve in the course of time, the function of sorption is thus arbitrarily selected.

1.3 Boundary conditions and loadings

In this test, drying and the temperature are supposed to be uniform and invariants. Moisture is worth 100% and the temperature $20^\circ C$.

The mechanical loading corresponds to an one-way traction on the higher face of the test-tube (P5P6P7P8) imposed into 1 second then maintained constant until reaching (almost) the ruin of material by tertiary creep. The intensity of the loading is equal to 0.6 times the instantaneous load of peak in the case of the coupling with ENDO_ISOT_BETON and 0.8 times the instantaneous load of peak for the coupling with MAZARS.

2 Reference solution

This test is a test of not-regression.

3 Modeling A

3.1 Characteristics of modeling

Modeling is 3D.

3.2 Characteristics of the grid

Many nodes: 8

Many meshes and types: 1 HEXA8

3.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 104), the constraint SIZZ, clean deformation of creep EPZZ like 2 internal variables V7 and V22 corresponding respectively to the reversible deviatoric deformation according to zz and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform).

Fields	Component	Not	Value of reference	Type of reference
SIEF_ELGA	SIZZ	Not Gauss 1	1.80000E+00	NON REGRESSION
VARI_ELGA	V5	Not Gauss 1	3.10881E-05	NON REGRESSION
VARI_ELGA	V22	Not Gauss 1	1.54698E-05	NON REGRESSION
EPSP_ELGA	EPYY	Not Gauss 1	5.57153E-05	NON REGRESSION

One in addition tests the weight of the point of Gauss 1.

Fields	Component	Not	Value of reference	Type of reference	Tolerance
COOR_ELGA	W	Not Gauss 1	0.25	ANALYTICAL	1e-7%

4 Modeling B

4.1 Characteristics of modeling

Modeling is axisymmetric (AXIS).

4.2 Characteristics of the grid

Many nodes: 4

Many meshes and types: 1 QUAD4

4.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 104), the constraint SIYY, clean deformation of creep EPYY like 2 internal variables V5 and V22 corresponding respectively to the reversible deviatoric deformation according to γ and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform).

Fields	Component	Not	Value of reference	Type of reference	Tolerance
SIEF_ELGA	SIZZ	Not Gauss 1	1.80000E+00	NON REGRESSION	0.01%
VARI_ELGA	V5	Not Gauss 1	3.10881E-05	NON REGRESSION	0.01%
VARI_ELGA	V22	Not Gauss 1	1.54698E-05	NON REGRESSION	0.01%
EPSP_ELGA	EPYY	Not Gauss 1	5.57153E-05	NON REGRESSION	0.01%

One finds the same results as in 3 dimensions.

5 Modeling C

5.1 Characteristics of modeling

Modeling is in plane constraints (C_PLAN).

5.2 Characteristics of the grid

Many nodes: 4

Many meshes and types: 1 QUAD4

5.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 104), the constraint SIYY, clean deformation of creep EPYY like 2 internal variables V5 and V22 corresponding respectively to the reversible deviatoric deformation according to $\gamma\gamma$ and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform).

Fields	Component	Not	Value of reference	Type of reference	Tolerance
SIEF_ELGA	SIZZ	Not Gauss 1	1.80000E+00	NON REGRESSION	0.01%
VARI_ELGA	V5	Not Gauss 1	3.10881E-05	NON REGRESSION	0.01%
VARI_ELGA	V22	Not Gauss 1	1.54698E-05	NON REGRESSION	0.01%
EPSP_ELGA	EPYY	Not Gauss 1	5.57153E-05	NON REGRESSION	0.01%

One in addition tests the weight of the point of Gauss 1.

Fields	Component	Not	Value of reference	Type of reference	Tolerance
COOR_ELGA	W	Not Gauss 1	0.25	ANALYTICAL	1e-7%

One finds the same results as in 3 dimensions.

6 Modeling D

6.1 Characteristics of modeling

Modeling is 3D.

6.2 Characteristics of the grid

Many nodes: 8

Many meshes and types: 1 HEXA8

6.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 202), the constraint SIZZ, like 2 internal variables V7 and V22 corresponding respectively to the reversible deviatoric deformation according to *zz* and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform). One also tests the value of displacement to the node N5 .

Fields	Component	Not	Value of reference	Type of reference	Tolerance
SIEF_ELGA	SIXX	Not Gauss 1	1.38880E +00	NON_REGRESSION	0.01%
DEPL	DX	N5	6.635E-5	NON_REGRESSION	0.01%
VARI_ELGA	V22	Not Gauss 1	5.607E-2	NON_REGRESSION	0.01%
VARI_ELGA	V7	Not Gauss 1	1.0145E-5	NON_REGRESSION	0.01%

7 Modeling E

7.1 Characteristics of modeling

Modeling is 2D in plane deformations D_PLAN.

7.2 Characteristics of the grid

Many nodes: 4

Many meshes: 1 QUAD 4

7.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 85), the constraint SIXX, like 2 internal variables V3 and V22 corresponding respectively to the reversible deviatoric deformation according to XX and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform). One also tests the value of displacement to the node NI .

Fields	Component	Not	Value of reference	Type of reference	Tolerance
SIEF_ELGA	SIXX	Not Gauss 1	1.38880E +00	NON_REGRESSION	0.01%
DEPL	DX	NI	-6.813E-3	NON_REGRESSION	0.01%
VARI_ELGA	V22	Not Gauss 1	7.466E-2	NON_REGRESSION	0.01%
VARI_ELGA	V3	Not Gauss 1	1.015E-5	NON_REGRESSION	0.01%

8 Modeling F

8.1 Characteristics of modeling

Modeling in plane constraints C_PLAN.

8.2 Characteristics of the grid

Many nodes: 4

Many meshes: 1 QUAD 4

8.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 85), the constraint SIXX, like 2 internal variables V3 and V22 corresponding respectively to the reversible deviatoric deformation according to \overline{XX} and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform). One also tests the value of displacement to the node NI .

Fields	Component	Not	Value of reference	Type of reference	Toleranc e
SIEF_ELGA	SIXX	Not Gauss 1	1.38880E +00	NON_REGRESSION	0.01%
DEPL	DX	NI	-6.5657E-3	NON_REGRESSION	0.01%
VARI_ELGA	V22	Not Gauss 1	4.2817E-2	NON_REGRESSION	0.01%
VARI_ELGA	V3	Not Gauss 1	9.4824E-6	NON_REGRESSION	0.01%

9 Modeling G

9.1 Characteristics of modeling

Not-local modeling 3D_GRAD_EPSI.

9.2 Characteristics of the grid

Many nodes: 20

Many meshes: 1 mesh HEXA 20

9.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 202), the constraint SIZZ, like 2 internal variables V7 and V22 corresponding respectively to the reversible deviatoric deformation according to zz and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform). One also tests the value of displacement to the node N5 .

Fields	Component	Not	Value of reference	Type of reference	Tolerance
SIEF_ELGA	SIXX	Not Gauss 1	1.38880E +00	NON_REGRESSION	0.01%
DEPL	DZ	N5	6.633E-05	NON_REGRESSION	0.01%
VARI_ELGA	V22	Not Gauss 1	5.5810E-2	NON_REGRESSION	0.01%
VARI_ELGA	V7	Not Gauss 1	1.0145E-05	NON_REGRESSION	0.01%

10 Modeling H

10.1 Characteristics of modeling

Not-local modeling 2D in deformation plane D_PLAN_GRAD_EPSI.

10.2 Characteristics of the grid

Many nodes: 8

Many meshes: 1 QUAD 8

10.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 85), the constraint SIXX, like 2 internal variables V3 and V22 corresponding respectively to the reversible deviatoric deformation according to XX and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform). One also tests the value of displacement to the node NI .

Fields	Component	Not	Value of reference	Type of reference	Tolerance
SIEF_ELGA	SIXX	Not Gauss 1	1.38880E +00	NON_REGRESSION	0.01%
DEPL	DX	NI	3.2017E-03	NON_REGRESSION	0.01%
VARI_ELGA	V22	Not Gauss 1	0.0	NON_REGRESSION	0.01%
VARI_ELGA	V3	Not Gauss 1	1.0653E-05	NON_REGRESSION	0.01%

11 Modeling I

11.1 Characteristics of modeling

Not-local modeling in plane constraints C_PLAN_GRAD_EPSI.

11.2 Characteristics of the grid

Many nodes: 8

Many meshes: 1 QUAD 8

11.3 Sizes tested and results

One tests with the last step of time (NUME_ORDRE 85), the constraint SIXX, like 2 internal variables V3 and V22 corresponding respectively to the reversible deviatoric deformation according to XX and the value of the damage. These sizes are observed on the first point of Gauss (all fields being uniform). One also tests the value of displacement to the node $N2$.

Fields	Component	Not	Value of reference	Type of reference	Toleranc e
SIEF_ELGA	SIXX	Not Gauss 1	1.38880E +00	NON_REGRESSION	0.01%
DEPL	DX	$N2$	3.1603E-03	NON_REGRESSION	0.01%
VARI_ELGA	V22	Not Gauss 1	0.0	NON_REGRESSION	0.01%
VARI_ELGA	V3	Not Gauss 1	9.1621E-06	NON_REGRESSION	0.01%

12 Synthesis

All these tests are tests of not-regression, which validate the establishment of the models from a point of view data-processing and not physical. Thus, on tests of enclosure, it was noticed that the coupling of the model ENDO_ISOT_BETON with BETON_UMLV_FP in the current version much the damage over-estimated.

In addition, one holds to inform the user, that the current coupling of the model of MAZARS with BETON_UMLV_FP is explicit and is thus sensitive in keeping with step of time used. A study of convergence is thus essential.