

## SSNV220 - Validation of modeling GVNO and the law of behavior ENDO\_CARRE in 3D

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This test allows the validation of modeling GVNO in 3D , which makes it possible to carry out the calculations of damage regularized by the gradient of the damage, by taking into account only degrees of freedom of displacement and damage to the nodes. The resolution of the criterion is total, unlike modeling GRAD\_VARI who carries out a local resolution, points of Gauss by points of Gauss. One validates simultaneously the law of behavior ENDO\_CARRE, of quadratic formulation in damage, which is for the moment the law that one can use with modeling GVNO.

## 1 Problem of reference

### 1.1 Tally theoretical

The unknown factors of the problem are the degrees of freedom of nodal displacement and damage. It is then a question of minimizing an energy of the form:

$$\phi(u, \alpha) = \frac{1}{2} A(d) E \epsilon^2 + \psi(d) + \frac{c}{2} \nabla \alpha \cdot \nabla \alpha$$

Where  $E$  is the Young modulus of material,  $A(d)$  the function of rigidity,  $\psi(d)$  dissipation and  $c$  the nonlocal coefficient.

In the case of the law ENDO\_CARRE :

$$A(d) = (1-d)^2 \quad \text{and} \quad \psi(d) = \frac{\sigma_y^2}{E} d$$

The criterion corresponding to the law ENDO\_CARRE, for a homogeneous solution ( $\nabla \alpha = 0$ ), is thus written:

$$d = 1 - \left( \frac{W_y}{W_{el}} \right)$$

Where  $W_{el}$  is the elastic deformation energy and:

$$W_y = \frac{\sigma_y^2}{2E}$$

### 1.2 Geometry

A cube on side is considered  $L = 1 \text{ m}$ .

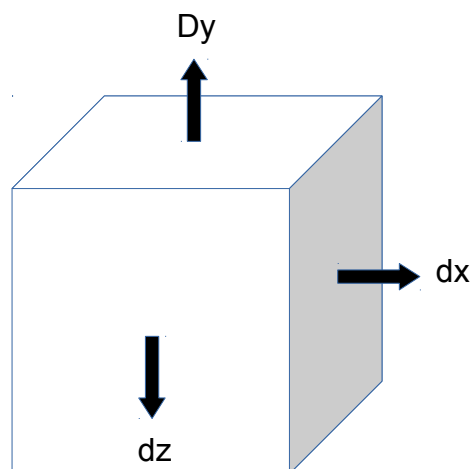


Figure 1 : Representation of the problem

## 1.3 Properties of material

Law of damage: material ENDO\_CARRE

Characteristics rubber bands:

$$E = 1 \text{ Pa}$$

$$\nu = 0.$$

Characteristics related to the law of damage:

Elastic limit:

$$SY = 0.01 \text{ Pa}$$

Not-local characteristics:

$$c = 1.0 \text{ N}$$

## 1.4 Boundary conditions and loadings

**Embedding** : Worthless imposed displacements  $DY = 0 \text{ m}$  . on the face of bottom (  $y=0.$  ),  $DX = 0 \text{ m}$  . on the left face (  $x=0.$  ) and  $DZ = 0 \text{ m}$  . on the face postpones (  $z=0.$  ) . See figure 1.

**Loading 1** : Imposed linear displacement  $U_1$  on the right face (  $x=1.$  ) :

$$U_1 = 0.0 \text{ m for INST}=0, U_1 = 0.02 \text{ m for INST}=1.0.$$

**Loading 1** : Imposed linear displacement  $U_2$  on the right face (  $y=1.$  ) :

$$U_2 = 0.0 \text{ m for INST}=0, U_2 = 0.02 \text{ m for INST}=1.0.$$

**Loading 1** : Imposed linear displacement  $U_3$  on the right face (  $z=1.$  ) :

$$U_3 = 0.0 \text{ m for INST}=0, U_3 = 0.02 \text{ m for INST}=1.0.$$

## 2 Reference solution

The imposed loadings enable us to obtain a homogeneous solution. The principal directions being clean directions of the tensor of the deformations, elastic energy results from the loadings defined previously in the following way:

$$W_{el} = \frac{(U_1^2 + U_2^2 + U_3^2)}{2L^2}$$

One extracts the associated values of damage analytically from them:

$$d = 1 - \left( \frac{2W_y L^2}{U_1^2 + U_2^2 + U_3^2} \right)$$

It is considered whereas the test is checked if Newton returns us well the same values of damage, with a precision of  $10^{-6}$  .

## 3 Modeling

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### 3.1 Characteristics of modeling

A modeling is used 3D\_GVNO.

### 3.2 Characteristics of the grid

The grid contains 64 elements HEXA20.

### 3.3 Results

NUMBER	TYPE_REFERENCE	VALE_REF	SHEET
1	'ANALYTICAL'	0.1	1.0E-4%
2	'ANALYTICAL'	0.5	1.0E-4%
3	'ANALYTICAL'	0.7	1.0E-4%
4	'ANALYTICAL'	0.85	1.0E-4%

**Table 1: Comparison of eigenvalues in room and not-room**

## 4 Summary of the results

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We get the results of references, with the precision requested, which validates modeling GVNO and the law of behavior ENDO\_CARRE in 3D.