

TTLV100 - Thermal shock in a pipe with condition of exchange

Summary:

This test of transitory linear thermics consists in imposing a cold thermal shock on a presumedly infinite hollow roll using a limiting condition of exchange.

The shock is modelled by a linear slope $\Delta T = -269^\circ C$ in $12s$.

With the problem is dealt into axisymmetric and 3D.

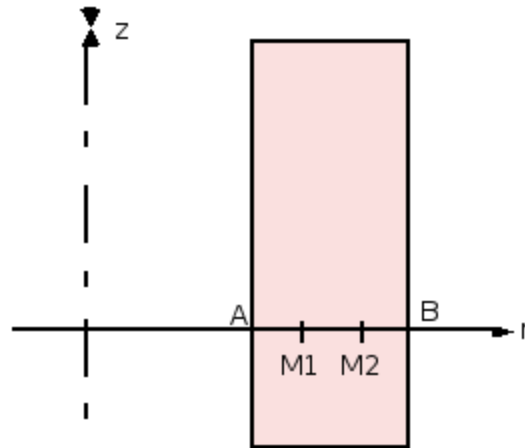
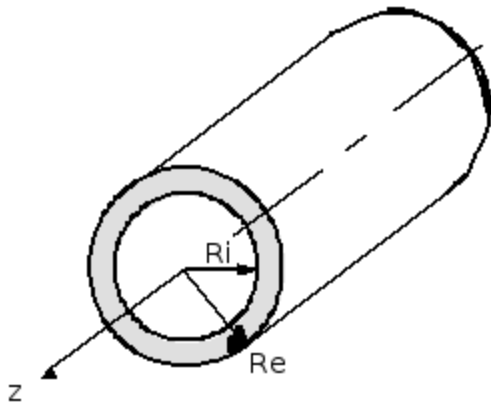
The reference solution is obtained on a fine network.

The test is carried out on 3 modelings: (TRIA3, QUAD4), (TRIA6, QUAD9) in AXIS_DIAG and (HEXA8, PENTA6) in 3D_DIAG.

One tests the algorithm of linear thermics transitory when the matrix of mass is diagonalisée (modeling AXIS_DIAG and 3D_DIAG with "farmhouse lumping").

1 Problem of reference

1.1 Geometry



$$R_i = 417 \text{ mm}$$

$$R_e = 496 \text{ mm}$$

$$r(A) = 417 \text{ mm}$$

$$r(B) = 496 \text{ mm}$$

$$r(M1) = 443.43 \text{ mm}$$

$$r(M2) = 469.67 \text{ mm}$$

1.2 Material properties

$$\lambda = 19.97 \text{ W/m}^\circ\text{C}$$

$$\rho C_p = 4.89488 \cdot 10^6 \text{ J/m}^3 \cdot ^\circ\text{C}$$

1.3 Boundary conditions and loadings

$$\text{Exchange } \lambda \frac{\partial T}{\partial n} \Big|_{r=r_i} = h (T_{ext} - T(r, t))$$

$$h = 40000 \text{ W/m}^2 \cdot ^\circ\text{C}$$

with $T_{ext}(A)_{t=0s} = 289 \text{ }^\circ\text{C}$

$$T_{ext}(A)_{t=12s} = 20 \text{ }^\circ\text{C}$$

1.4 Initial conditions

$$T(r, 0) = 289 \text{ }^\circ\text{C} \quad \text{for all } r$$

Discretization in time (t) :

12	not for	[0., 12.]	that is to say	$\Delta t = 1.s$
2	not for	[12., 20.]	that is to say	$\Delta t = 4.s$
4	not for	[20., 100.]	that is to say	$\Delta t = 20.s$

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2	not for	[100., 200.]	that is to say	$\Delta t = 50.s$
2	not for	[200., 400.]	that is to say	$\Delta t = 100.s$
8	not for	[400., 2000.]	that is to say	$\Delta t = 200.s$

2 Reference solution

2.1 Method of calculating used for the reference solution

The reference solution is obtained on a fine network comprising 99 quadratic elements QUAD8 in the thickness without option of matrix of diagonal thermal mass.

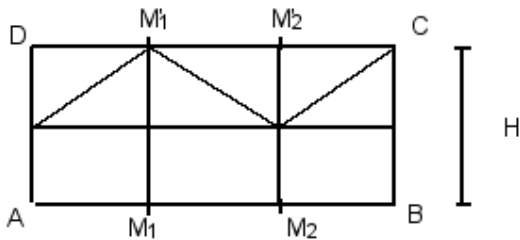
2.2 Results of reference

Temperatures at the points $M1$ ($r=443.33$) and $M2$ ($r=469.67$), and at various moments ($t=12.$, $100.$, $600.$ and $2000.$).

3 Modeling A

3.1 Characteristics of modeling

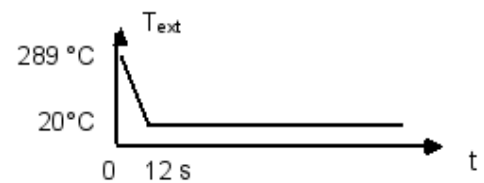
The infinite cylinder being supposed, one nets only one slice height $H = 40\text{ mm}$ with 2 layers of elements.



Conditions limites

sur [AB], [BC] et [CD] : flux nul

sur [AD] : échange h, T_{ext}



points	nœuds	r	z
M1	N10	443.33	0.0
M2	N5	469.67	0.0
M'1	N11	443.33	40.
M'2	N7	469.67	40.

Conditions initiales
 $T = 289\text{ °C}$

3.2 Characteristics of the grid

Many nodes: 12

Many meshes and types: 3 QUAD4, 6 SORTED3

3.3 Sizes tested and results

Identification	Type of reference	Value of reference	Precision (%)
M1 (R = 443.33)			
T = 12.	'AUTRE_ASTER'	288.64	0.5
T = 100.	'AUTRE_ASTER'	202.76	0.1
T = 600.	'AUTRE_ASTER'	93,027	0.1
T = 2000.	'AUTRE_ASTER'	29,419	0.1
M2 (R = 469.67)			
T = 12.	'AUTRE_ASTER'	289.00	0.1
T = 100.	'AUTRE_ASTER'	275.04	0.5
T = 600.	'AUTRE_ASTER'	143.00	0.1
T = 2000.	'AUTRE_ASTER'	35,858	0.5
Me 1 (R = 443.33)			
T = 12.	'AUTRE_ASTER'	288.64	0.5
T = 100.	'AUTRE_ASTER'	202.76	0.1
T = 600.	'AUTRE_ASTER'	93,027	0.1
T = 2000.	'AUTRE_ASTER'	29,419	0.1

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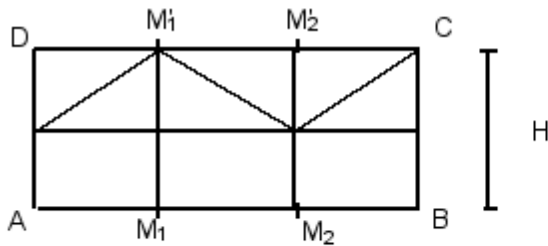
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Me 2 (R = 469.67)			
T = 12.	'AUTRE_ASTER'	289.00	0.1
T = 100.	'AUTRE_ASTER'	275.04	0.5
T = 600.	'AUTRE_ASTER'	143.00	0.1
T = 2000.	'AUTRE_ASTER'	35,858	0.5

4 Modeling B

4.1 Characteristics of modeling

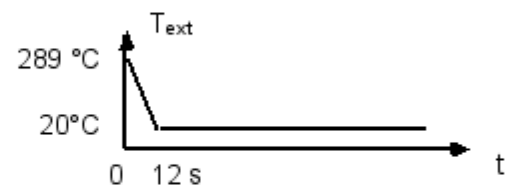
The infinite cylinder being supposed, one nets only one slice height $H = 40\text{ mm}$ with 2 layers of elements.



Conditions limites

sur [AB], [BC] et [CD]: flux nul

sur [AD]: échange h, T_{ext}



points	nœuds	r	z
M1	N25	443.33	0.0
M2	N9	469.67	0.0
M'1	N28	443.33	40.
M'2	N1	469.67	40.
6			

Conditions initiales
 $T = 289\text{ °C}$

4.2 Characteristics of the grid

Many nodes: 35

Many meshes and types: 3 QUAD9, 6 TRIA6

4.3 Sizes tested and results

Identification	Type of reference	Value of reference	Precision (%)
M1 (R = 443.33)			
T = 12.	'AUTRE ASTER'	288.64	0.5
T = 100.	'AUTRE ASTER'	202.76	0.1
T = 600.	'AUTRE ASTER'	93,027	0.1
T = 2000.	'AUTRE ASTER'	29,419	0.1
M2 (R = 469.67)			
T = 12.	'AUTRE ASTER'	289.00	0.1
T = 100.	'AUTRE ASTER'	275.04	0.5
T = 600.	'AUTRE ASTER'	143.00	0.1
T = 2000.	'AUTRE ASTER'	35,858	0.5
Me 1 (R = 443.33)			
T = 12.	'AUTRE ASTER'	288.64	0.5
T = 100.	'AUTRE ASTER'	202.76	0.1
T = 600.	'AUTRE ASTER'	93,027	0.1
T = 2000.	'AUTRE ASTER'	29,419	0.1

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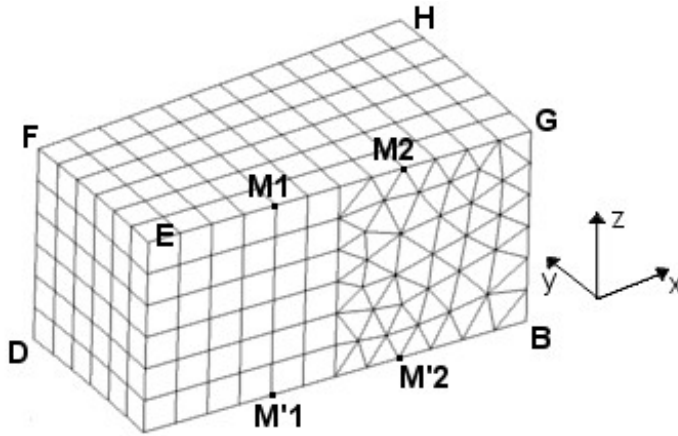
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Me 2 (R = 469.67)				
T = 12.	'AUTRE_ASTER'	289.00		0.1
T = 100.	'AUTRE_ASTER'	275.04		0.5
T = 600.	'AUTRE_ASTER'	143.00		0.1
T = 2000.	'AUTRE_ASTER'	35,858		0.5

5 Modeling C

5.1 Characteristics of modeling

The infinite cylinder being supposed, one nets only one slice height $H = 40 \text{ mm}$.

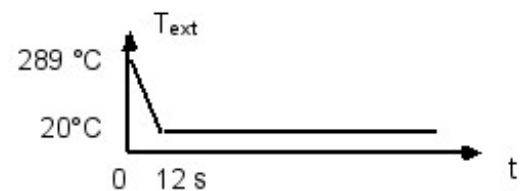


points	nœuds	x	y	z
M1	N179	443.33	0.0	20.0
M2	N616	469.67	0.0	20.0
M'1	N384	443.33	0.0	-20.0
M'2	N325	469.67	0.0	-20.0

Conditions limites

sur face [AEFD] : échange h, T

sur les autres faces : flux nul



Conditions initiales
T = 289 °C

5.2 Characteristics of the grid

Many nodes: 637

Many meshes and types: 216 HEXA8, 432 PENTA6

5.3 Sizes tested and results

Identification	Type of reference	Value of reference	Precision (%)
Max (TEMP) – GROUP_NO 'M1'	'ANALYTICAL'	289.0	0.1
M1 (R = 443.33)			
T = 12.	'AUTRE_ASTER'	288.64	0.5
T = 100.	'AUTRE_ASTER'	202.76	0.1
T = 600.	'AUTRE_ASTER'	93,027	0.1
T = 2000.	'AUTRE_ASTER'	29,419	0.1
M2 (R = 469.67)			
T = 12.	'AUTRE_ASTER'	289.00	0.1
T = 100.	'AUTRE_ASTER'	275.04	0.5
T = 600.	'AUTRE_ASTER'	143.00	0.1
T = 2000.	'AUTRE_ASTER'	35,858	0.5
Me 1 (R = 443.33)			
T = 12.	'AUTRE_ASTER'	288.64	0.5
T = 100.	'AUTRE_ASTER'	202.76	0.1

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T = 600.	'AUTRE_ASTER'	93,027	0.1
T = 2000.	'AUTRE_ASTER'	29,419	0.1
<hr/>			
Me 2 (R = 469.67)			
T = 12.	'AUTRE_ASTER'	289.00	0.1
T = 100.	'AUTRE_ASTER'	275.04	0.5
T = 600.	'AUTRE_ASTER'	143.00	0.1
T = 2000.	'AUTRE_ASTER'	35,858	0.5

6 Summary of the results

Modeling `AXIS_DIAG` give rather satisfactory results. Although the grid comprises only 3 elements in the thickness, the variation on the temperatures remains lower than 0.5 %.

Modeling `3D_DIAG` give satisfactory results. The variation on the temperatures remains too lower than 0.5 %.

In spite of the violence of the thermal shock, the diagonalisation of the matrix of mass allows thus to obtain a solution in temperature which does not oscillate during the transient.